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RELIABLE, LOW COST, STABLE RESISTORS

GENERAL PURPOSE

REPORT #10

CONTRACT NO.: DA-36-039-AMC-02202(E)
DA TASK NO.: 1P6 22001-A 057 01
ORDER NO.: 5465-PM-63-91

Tenth Quarterly Progress Report 1 August 1965 to 31 October 1965

Prepared for the U. S. Army Electronics Command

Fort Monmouth, New Jersey

by

I R C

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RELIABLE, LOW COST, STABLE RESISTORS

GENERAL PURPOSE

REPORT #10

Contract No.: DA-36-039-AMC-02202 (E)

Applicable Specifications: SCL-2101P 18 February 1963
"Technical Reports"
Technical Guidelines, 7 February, 1964
Reliable, Low Cost, Stable Resistor
MIL-R-11/8, 17 May 1963


Order No.: 5465-PM-63-91

Tenth Quarterly Progress Report 1 August 1965 to 31 October 1965

Objective: Reliability Evaluation and Improvement of
Stable, Low Cost, General Purpose Resistors.

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PURPOSE

For many years, the "workhorse" among electronic components has been the general purpose carbon composition resistor. The quality, reliability, and stability of this component has been improving for many, many years; this has been reflected in the increasing tightness of the requirements for its performance, as spelled out in subsequent revisions of its applicable specification, MIL-R-11. The resistor is inexpensive, is readily available, and its application reasonably well understood by circuit designers.

With the ever increasing complexity of military electronic equipments, and with the increasing demands for products that perform under higher environmental stresses, an increasing need is developing for a component with performance characteristics superior to the familiar composition resistor. In recognition of this fact, International Resistance Company has carried on development work on two new resistive systems. One of these was based on conductive ceramic in bulk form; the other makes use of a class of resistive materials known as glazes or cermets, utilized in the form of a film or coating on a substrate.

These two units were evaluated as general purpose resistors meeting the stated needs. The evaluation indicated that a resistor combining the glaze resistive film with the assembly methods of the bulk unit had an excellent chance of meeting these requirements. Such a resistor has been developed. It is intended that it be evaluated against the specified needs and that further development work be done as required to assure the availability of such a unit.

ABSTRACT

MIL-R-11 70 °C load life tests have been completed to 1000 hours on the 100Ω group. The completed results, on all pertinent resistance values, demonstrates conformance to the MIL-R-11 requirements. The contract requirements of 5% maximum resistance change on the Mli moisture resistance and Resistance-Temperature characteristic of less than 500ppm/°C have also been met.

The moisture load matrix has been completed through 2000 hours on the 100Ω and 100KΩ groups. These results definitely indicate smaller resistance changes with increasing load, especially in the 100KΩ group.

The temperature load matrix tests have completed 2000 hours on the 100Ω group and 3000 hours on the 100KΩ group. The 10Ω, 1KΩ, 10KΩ, and 39KΩ groups have completed 6000 hours of testing. The present calculated failure rate, which includes the two early (50 hours of test) failures on the 100KΩ group, is 0.10%/1000 hours at a confidence level of 60%, on units tested at 85 °C ambient with 1/4 watt load. The calculated failure rate without the two early failures is no more than 0.03%/1000 hours at a confidence level of 60%. The average resistance change for the 100Ω and 100KΩ groups after 2000 hours at 85 °C ambient with 1/4 watt load is less than 0.1%; and less than 0.4% on the 10Ω, 1KΩ, 10KΩ, and 39KΩ groups.

BACKGROUND

The Rv resistor consisted of a completely inorganic volume resistive element with metallized termination and a molded jacket. It was fabricated in resistance values from 2.7Ω to $30,000\Omega$ in the form factor of the RC-07 style of MIL-R-11E. The resistor demonstrated excessive resistance changes when subjected to high humidity and D.C. load and was not capable of meeting the required $.05\%/^{\circ}\text{C}$ resistance-temperature characteristic. Equipment capable of low cost production of this unit was designed.

The L07 resistor utilizes a metal glaze fired on a ceramic substrate. Silver terminations are fired on to the ends, a ground helix in the metal glaze is used to determine resistance value and cap leads are pressed on the ends of the body. A filled modified silicone coating material is used to provide electrical insulation and mechanical protection. The use of cap leads and (to a lesser extent) precious metal glaze, coupled with repeated price reductions in the composition resistor market, have made it impossible for this resistor to be considered as being in the same price range as the MIL-R-11E composition resistors. In addition, the general construction, and particularly the use of cap leads, makes any substantial size reduction in this unit (as specified in the Technical Guidelines) for lower power use extremely unlikely.

Because of the specific problems encountered in the Rv and L07 units a third approach termed the Rg has been implemented. This consists of a metal glaze fired on a ceramic substrate and toleranced by helixing as in the L07 process. The termination and molded jacket are those used on the Rv. The low cost processes and automated equipment of the Rv are used throughout the Rg process with the exception of the glaze application firing and helixing steps which utilize automated L07 type equipment.

This approach is expected to result in a resistor with the excellent performance of the L07 combined with the price and size reduction potential of the Rv.

FACTUAL DATA

I. Temperature Load Matrix

The current failure rate curve is shown in Figure I. As can be seen, no failures have occurred since the last report indicating a failure rate of not more than 0.1%/1000 hours at a confidence level of 60%. As stated before tests were run to determine the possibility of the two failures reported in Report #9 were mechanical failures. The failure rate without these two failures is shown on the curve with a broken line. This curve indicates a failure rate of no more than 0.03%/1000 hours at a confidence level of 60%.

Up to 6000 test hours have now elapsed for the resistance values (10 Ω , 1K Ω , 10K Ω , & 39K Ω) 2000 hours for 100 Ω and 3000 hours for 100K Ω in the temperature load matrix. An up-to-date summary of test results are shown in Tables I and II.

It was originally planned that 21 of the 30 cells in the load life matrix would run for only 2000 hours and that the balance would be run for the full 10,000 hours. The resistance changes and the incidence of failure after 2,000 hours under stresses as high as 150 °C, 3/4 watt, were so small as to prevent derivation of a mathematical model of Rg performance. For this reason all cells were continued to the 5000 hour point. This has been reached for the 10 Ω , 1K, 10K and 39K groups and these have been removed. Failures in these groups will be analyzed in an effort to determine failure mode.

Work has started on the development of a degradation model for resistance values, 1K Ω & 10K Ω . A computer program was written to retrieve test data from a history tape and perform a linear regression of % Δ R vs. time for each block of the test matrix. The program has been run successfully and up to the writing of this report, the slopes, (rate of resistance change with respect to time) were being evaluated graphically for possible fit to the Arrhenius or Eyring rate of reaction models. If the graphical analysis yields reasonably good results, the data will be evaluated more accurately with a least square multiple regression program. The only thing that can be reported at this time for resistance values, 1K Ω , & 10K Ω is that % resistances for practically every stress condition has a highly significant linear relationship with time. More detailed results should be available for the next quarterly report.

Frequency plots of $\% \Delta R$ readings at indicated 1000 hour intervals for 85°C 1/4 watt stress conditions are shown in Figures 2 through 9. The 100 Ω & 100K Ω values, Figures 10 through 14 show very tight normal distributions and low average resistance changes. Resistance values, 10 Ω , 10K Ω & 39K Ω have a few outliers, low average resistance changes and no failures, (greater than 5.0%). The 100K Ω value also has a number of outliers with two of them being failures. At 1000 hours, one resistor read -12.65% and at 2000 hours another resistor read -5.35%. At 3000 hours the -12.65% resistor recovered to -0.47%. These two failures were discussed under the failure rate progress section of the last Quarterly Report.

For an explanation of an interpretation of the values under calculations/summary shown on each plot, refer to the previous Quarterly Report.

A total of 2,580 resistors are included in the portion of the temperature load matrix which does not represent an overload to a rating of 1/4 watt at 85°C. Of these resistors, six have exhibited resistance changes greater than 5% and can therefore be considered performance failures. Of the six failures, four were early failures which occurred during the first 100 hours of load. The remaining two occurred under no load conditions. Experience on other resistors under high reliability specifications (such as MIL-R-55182) indicates that a burn in under load conditions is necessary to eliminate early failures. Thus resistors subject to the early failure mode may ultimately fail under no load conditions, but are not particularly likely to fail early in the test. In this context, the fact that the incidence of failure in the no load cells (2/900) is the same as the incidence of early failure (4/1860) in the load cells, suggests that the same weakness is involved in both.

The history gathered on the Rg 1/4 watt with reference to the STOL (short time overload) screen vs. the test data indicated that "sporty" test rejects could be eliminated by screening the units with an overload prior to testing. The standard MIL-R-11E STOL test was instituted as a production operation with good results. From time to time, as in the contract data, lot samples on test would yield "sporty" failures which could be traced to improper screening. These incidents were few, however. An initial evaluation was set up to again prove that the failures shown on the contract could be traced to possible insufficient screening. If this can be demonstrated, it would be possible to eliminate these early failures as process failures not a normal failure rate problem.

A lot of standard low metal content 100K Rg rods was processed through molding as per standard procedures except for STOL. These units were split into two groups. One group received the no STOL and one STOL one at a time with readings before and after STOL. Units which changed more than 2.5% were eliminated from the screened groups. It should be noted that there were (13) thirteen such rejects.

All units were placed on 85°C 1/4 watt load life for 48 hours. The results of the load life ΔR 's were plotted and are shown of Figure #15 attached. As can be seen from these plots, the No STOL group has more "sports" than does the STOL group. In order to determine the significance of these two plots the data was given further analysis as below.

Figures #16 and #17 show the cumulative frequencies of the two distributions as plotted on Weibull Probability paper. Constants were added to the individual ΔR 's in order to make all results positive. The reason for these plots is to find the cut-off point for the outliers or "sports". Had these been single distributions, the lines would be straight. The break-off points from the plots indicated (12) twelve "sports" for the No STOL group, against (3) for the STOL group. The probability of obtaining 12/230 vs. 3/300 in two samples that were known to have been randomly selected from the same population was calculated using the following formula:

$$P = \frac{A!}{a!} \frac{B!}{b!} \frac{R!}{(A-a)!} \frac{(N-R)!}{(B-b)!} \frac{1}{N!}$$

Where A = Sample size of 1st sample = 230
 B = " " " 2nd sample = 300
 a = No. of outliers in 1st sample = 12
 b = " " " 2nd sample = 3
 N = A + B = 530
 ! = Factorial
 R = a + b = Total of outliers

The results of these calculations shows a low probability (on the order of .03) below the .05 significance level that the two samples are not significantly different. Therefore, it can be said that the two distributions are significantly different. It can therefore be assumed that proper screening will reduce early failures and for this reason failure rate calculations will continue to be made with and without early failures.

A screen test evaluation will be conducted using 510Ω and 150K resistors and the following screening conditions:

1. Control (no screening)
2. 2 1/2 times rated voltage for 5 seconds
3. 3 1/2 times rated voltage for 5 seconds
4. 2 1/2 times rated voltage for 60 seconds
5. 1/2 watt at 70°C for 8 hours

The resistors which remain within ±2% of their original resistance value will be submitted to 1/4 watt load for 96 hours at 85°C. Resistance readings will be made after 1, 2, 3, 4, 8, 24, 48 and 96 hours.

II. Step-Stress Test Matrix

The step-stress program as outlined in the last report has been completed. However, the data has not as yet been completely analyzed. There is, however, data completed on the temperature rise measurements. This is discussed below.

III. Temperature Rise Measurements

As is well known, a current flowing through a resistor will generate a temperature rise in the resistor and create a hot-spot. This temperature rise is a function of such things as the diameter and length of the resistor body, length and diameter of leads, dissipated power, ambient temperature, heat transfer and heat conduction coefficients. For the Rg resistor a mathematical expression of temperature rise as a function of power dissipation and load was developed from measurements taken on (2) resistors each from resistance values (10Ω, 100Ω, 1KΩ, 10KΩ, 39KΩ and 100KΩ) under loads (1/8, 1/4, 3/8, 1/2, 5/8, 3/4, and 1 watt) and ambient temperatures (70 °C, 100 °C, 125 °C, and 150 °C). These temperature rise (Δ T), measurements are listed in Figures #18 through #21.

Using graphical means, an expression of the following form was obtained.

$$\Delta T = L (85 - 0.18 T) \quad (1)$$

(8)

Where

ΔT = Temperature Rise in $^{\circ}\text{C}$

L = Load in Watts

T = Ambient Temperature in $^{\circ}\text{C}$

A plot of temperature rise curves for the various ambients are shown in Figure #22.

Dissipation constants, (D), in terms of milliwatts per degree C a measure of the power required to raise the resistor temperature 1°C can be calculated from the following derived equation (3).

$$D = \frac{L}{\Delta T} \quad (2)$$

On substituting EQ (1) in (2) and multiplying by 1000 to obtain mw/ $^{\circ}\text{C}$, it follows,

$$D = \frac{1}{85 - 0.18T} \times 1000 \quad (3)$$

Dissipation constants for each ambient are listed below:

<u>Ambient</u>	<u>Dissipation Constant (mw/$^{\circ}\text{C}$)</u>
70 $^{\circ}\text{C}$	13.81
100 $^{\circ}\text{C}$	14.92
125 $^{\circ}\text{C}$	16.00
150 $^{\circ}\text{C}$	17.24

The difference in dissipation constants for the different ambients is attributed to a dependence of the heat transfer coefficients between the resistor, and its environment, upon the ambient temperature.

IV. Physics of Resistance Change

The mechanism of resistance change for the Rg resistor under thermal stress was explained in a previous report as due to a combination annealing and oxidation process. The initial negative drifts observed for different temperature load stresses was attributed an annealing process. The shift from negative

to positive resistance changes was attributed to an oxidation mechanism, presumably of the metal particles in the glaze.

To substantiate the annealing and oxidation mechanisms, the following experiment was performed:

- (a). (60) 10K Ω resistors were randomly selected from a homogeneous lot and divided into two randomly selected groups.
- (b). One group was placed with no load in an air atmosphere oven set at 175°C. The other group was placed with no load in an oven set at 175°C wherein argon was slowly forced through.
- (c). Resistance measurements were taken at selected intervals and recorded.
- (d). After the end of 2000 hours, the resistors in argon were transferred to the oven with the air atmosphere.

The results from the experiment are now complete and indirectly support the proposed mechanism for resistance change. Shown in Figures #23 and #24 are distribution plots of $\% \Delta R$'s for the two groups. The group in air shows a negative drift followed by a positive drift to an average ΔR of +1.37% after 2000 hours. The group in argon shows a gradual negative drift to -1.58% after 2000 hours. These results are interpreted as follows:

The units in argon underwent an annealing process only since they were not exposed to oxygen from the air, whereas the resistors in air underwent both an annealing and oxidation process.

After being placed in air, the resistors initially in argon started to drift positive to an average of +0.93% after 1800 hours as plotted in Figure #24. This again indicates an oxidation process taking place. The oxidation process as compared to annealing appears to be influenced more by production variations of glaze thickness, firing conditions, substrate differences and etc. This is evidenced by the larger $\% \Delta R$ dispersions shown by the resistors while in air.

The same experiment is being replicated using 1K Ω resistors. The data collected so far indicates a similar pattern taking place.

V. MIL-R-11 Tests

The MIL-R-11 data summary Figures #25 and # 26 is now completed on the six pertinent resistance values. The additional data to be reported is the completion of 1000 hours of 70 °C Load Life tests on the 100Ω group which shows a maximum change of -0.28%. Completion of the MIL-R-11 E testing has demonstrated the capability of the Rg-1/4 resistor over the resistance range values from 100Ω to 100KΩ. The Rg-1/4 has also successfully demonstrated its capability to be well within the requirements of 0.05%/°C temperature characteristic and ±5% maximum resistance change on moisture resistance and load life test, as outlined in the Technical Guidelines.

VI. Moisture Load Matrix Tests

The moisture load matrix test is run at 98% - 100% relative humidity at 55°C at no load and with loads of 1/20 watt, 1/8 watt, and 1/4 watt, continuously applied. The test is intended to identify any conditions of moisture load stress which induce excessive resistance changes.

The moisture - load matrix has completed 2000 hours on the 100Ω and 100KΩ groups. A summary of the data is included in Figures #27 through #32.

The following is a discussion of the results for the 100Ω and 100KΩ groups. A resistance change of over 10% has been defined as a failure for this matrix.

1. No Load

100Ω group: No failures, maximum change ±2.63%

100K group: 7 failures, maximum change -16.49%

2. 1/20 Watt Load

100Ω group: No failures, maximum change +0.29%

100KΩ group: No failures, maximum change +6.82%

3. 1/8 Watt Load

100Ω group: No failures, maximum change 0.14%

100KΩ group: No failures, maximum change 0.91%

4. 1/4 Watt Load

100Ω group: No failures, maximum change +0.77%

100KΩ group: No failures, maximum change +0.82%

The moisture - no load block of this matrix has been identified for these resistance values as for those previously tested, to be the most severe condition. The failures resulting from these tests will be analyzed in an attempt to identify the mechanism of failure. However, a test condition of 98 - 100% R.H. at 75°C as used in the accelerated moisture tests may be more useful for an accelerated test of moisture resistance capability.

VII. Experimental Activities

The resistors from the original runs, made to achieve improved temperature coefficient, were submitted for full MIL-R-11 tests. The results of these tests are summarized in Figure #33. The 250Ω resistors were from the high metal content glaze; 1.5K from medium metal content glaze and 100KΩ from low metal content glaze. A complete conformance to MIL-R-11 is demonstrated by this data. In addition, the temperature coefficient are all within 200 ppm and the moisture resistance and load life resistance changes are well within the 5% maximum contract requirements.

The temperature coefficient results on the repeatability runs are plotted on Figure #34.

CONCLUSIONS

The Rg - 1/4 watt has demonstrated a complete conformance to the requirements of MIL-R-11E. In addition, this resistor has met the specific requirements of; resistance-temperature characteristic (less than 0.05%/°C), moisture resistance and load life (less than 5%), as outlined in the Technical Guidelines.

The calculated failure rate, on resistors tested at 85°C 1/4 watt load, 0.1%/ 1000 hours could be reduced to 0.03%/ 1000 hours by elimination of early failures. Early failures (within the first 100 hours after application of voltage) are the only type which have been observed in the 16 load cells (out of 25) in the matrix, which do not constitute severe overloads. In these cells (limited by the conditions 25°C at 3/4 watt, 70°C at 1/2 watt, 85°C at 1/2 watt, 125°C at 1/4 watt and 150°C at 1/8 watt) seven early failures have been observed during accumulation of 13, 000, 000 unit hours. Tighter controls on the production screen testing (STOL) indicate these early failures may be eliminated.

The excellent results in the 1/4 watt at 125°C load block of the temperature load matrix, demonstrate the capability of the Rg-1/4 resistor to operate at ambients in excess of 85°C.

PROGRAM FOR NEXT QUARTER

1. Continue failure rate curve for groups tested at 85°C ambient with 1/4 watt load.
2. Analysis of data from the step-stress test program, which consisted of applying loads in 1/8 watt steps from 1/8 watt to 1 watt at 70 °C, 100 °C, 125 °C, and 150 °C will be initiated.
3. Continue performing preliminary regression of $\% \Delta R$ vs. time for the 85 °C 1/4 watt block of temperature load matrix.
4. Continue mechanism of failure experiment on 1K Ω resistors, comparing performance in argon vs. air atmosphere.
5. Continue screen test evaluations.

PERSONNEL

<u>Department</u>	<u>Hours</u>
Rg Assembly	182.5
R&D / Engineering	1425.0
J. Brzeczek	155.5
M. Dixon	244.5
J. Forman	173.5
W. Hawk	266.5
P. Lowenstein	82.5
C. Mabie	22.5
S. Mattie	132.0
J. Saboe	67.5
N. Thelin	37.5
J. Troendle	228.0
R. Vander Harr	15.0
Environmental Test Laboratory	<u>651.3</u>
TOTAL	2258.8

The above represents time spent on the contract during the period 1 August 1965 through 31 October 1965.

APPENDIX

Table I (30 pages)	Temperature Load Matrix Summary (Original Submission)
Table II (35 pages)	Temperature Load Matrix Summary (Resubmitted 100 Ω and 100K Ω)
Figure 1	Failure Rate Curve
Figures 2 through 14	Frequency Distribution - 1/4 Watt 85°C Load Life
Figure 15	Load Life ΔR - STOL Screen Test
Figures 16 and 17	Cumulative Frequencies Distribution - Screen Test vs. Load Life
Figures 18 through 21	Temperature Rise vs. Load in Various Ambients
Figure 22	Temperature Rise Curves
Figures 23 and 24	Frequency Distributions - Annealing vs. Oxidation Experiment
Figures 25 and 26	MIL-R-11-E Data Summary
Figures 27 through 32	Moisture Load Matrix Summary
Figure 33	MIL-R-11 Performance Summary Improved T C Runs'
Figure 34	Temperature Coefficient Repeatability Runs

TABLE I TEMPERATURE LOAD - MATRIX

TEST 25°C - No Load

Fall. Limit $\pm 5.0\%$

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RANGE	HOURS												
	50	100	250	500	750	1000	2000	3000	4000	5000			
100	Avg.	-0.033	-0.047	-0.026	0.037	-0.010	0.179	-0.340	-0.328	-0.013			
	Max	0.200	0.100	0.100	0.300	0.300	1.314	0.100	0.100	1.021			
	Min	-0.496	-0.397	-0.397	-0.099	-0.421	-0.526	-0.900	-0.900	-0.695			
	Sigma	0.139	0.117	0.114	0.098	0.150	0.365	0.265	0.259	0.335			
	K-1	-1.280	-1.240	-1.540	0.696	-0.268	1.320	-0.470	-0.374	0.625			
	N	30	30	30	30	30	30	30	30	30			
	Fails	0	0	0	0	0	0	0	1	1			
1000	Avg.	0.018	0.002	0.032	0.061	0.063	0.176	0.058	0.128	0.108			
	Max	0.069	0.089	0.178	0.178	0.178	0.781	0.138	0.206	0.215			
	Min	0.000	-0.098	-0.029	-0.019	-0.029	0.009	-0.029	-0.009	0.000			
	Sigma	0.028	0.037	0.045	0.051	0.048	0.180	0.044	0.050	0.048			
	K-1	0.730	-0.260	1.260	0.321	0.110	-0.064	0.185	-0.344	0.067			
	N	30	30	30	30	30	30	30	30	30			
	Fails	0	0	0	0	0	0	0	0	0			
10000	Avg.	0.021	0.004	0.049	0.088	0.131	0.135	0.203	0.271	0.311			
	Max	0.095	0.097	0.161	0.213	0.282	0.311	0.395	0.499	0.612			
	Min	-0.097	-0.097	-0.097	-0.097	0.000	0.00	0.000	0.000	0.058			
	Sigma	0.046	0.051	0.062	0.067	0.069	0.068	0.101	0.126	0.141			
	K-1	-0.225	-0.220	0.573	-0.276	0.456	0.490	0.114	-0.007	0.156			
	N	30	30	30	30	30	30	30	30	30			
	Fails	0	0	0	0	0	0	0	0	0			
39000	Avg.	-0.013	0.013	0.045	0.080	0.104	0.109	0.156	0.229	0.317			
	Max	0.077	0.077	0.176	0.233	0.285	0.285	0.337	0.448	0.757			
	Min	-0.436	-0.025	-0.050	0.000	-0.076	0.000	0.038	0.083	-0.077			
	Sigma	0.083	0.093	0.044	0.054	0.070	0.068	0.070	0.118	0.186			
	K-1	-0.043	1.140	0.733	0.920	0.289	0.682	0.675	0.966	0.522			
	N	30	30	30	30	30	30	30	30	30			
	Fails	0	0	0	0	0	0	0	0	0			

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RANGE	HOURS							
								6000
	Avg.							
	Max							
	Min							
	Sigma							
	K-1							
	N							
	Falls							
	Avg.							0.238
	Max							0.511
1 HD	Min							0.089
	Sigma							0.103
	K-1							1.020
	N							30
	Falls							0
	Avg.							
	Max							
	Min							
	Sigma							
	K-1							
	N							
	Falls							
	Avg.							
	Max							
	Min							
	Sigma							
	K-1							
	N							
	Falls							
	Avg.							
	Max							
	Min							
	Sigma							
	K-1							
	N							
	Falls							
	Avg.							
	Max							

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[illegible]

TABLE I. TEMPERATURE-LOAD MATRIX

TEST 70°C - 1/8 Watt

Fall. Limit $\pm 5.0\%$

Page 8 of 30

RANGE	HOURS										
	50	100	250	500	7500	1000	2000	3000	4000	5000	
100	Avg.	0.037	-0.023	0.023	0.059	0.029	-0.006	0.180	0.239	0.306	0.272
	Max	0.513	0.000	0.398	0.298	0.398	0.398	0.604	0.697	0.991	0.991
	Min	-0.099	-0.099	-0.299	-0.099	-0.198	-0.198	-0.198	-0.299	-0.299	-0.299
	Sigma	0.123	0.042	0.114	0.132	0.093	0.114	0.185	0.215	0.287	0.288
	K-1	2.580	-1.260	0.594	2.530	1.300	0.909	0.568	0.238	0.588	0.806
	N	30	30	30	30	30	30	30	30	30	30
	Falls.	0	0	0	0	0	0	0	0	0	0
1000	Avg.	0.016	0.019	0.062	0.054	0.028	0.097	0.182	0.272	0.289	0.219
	Max	0.058	0.078	0.126	0.136	0.301	0.223	0.304	0.418	0.486	0.372
	Min	-0.009	-0.019	0.009	0.000	-0.295	0.019	0.097	0.195	0.195	0.096
	Sigma	0.023	0.026	0.031	0.039	0.122	0.051	0.054	0.057	0.072	0.076
	K-1	0.885	0.550	0.183	0.345	-0.843	0.550	0.458	0.910	1.050	0.443
	N	30	30	30	30	30	30	30	30	30	30
	Falls.	0	0	0	0	0	0	0	0	0	0
10000	Avg.	-0.052	0.007	0.120	0.183	0.215	0.267	0.389	0.453	0.653	0.697
	Max	0.087	0.124	0.344	0.430	1.674	0.669	0.956	1.089	2.449	1.480
	Min	-0.135	-0.191	-0.133	-0.047	0.000	0.000	0.153	0.172	-0.334	0.277
	Sigma	0.056	0.056	0.069	0.077	0.107	0.107	0.147	0.168	0.863	0.289
	K-1	0.411	-1.540	-0.577	0.199	4.220	1.270	1.940	1.690	2.070	1.399
	N	30	30	30	30	30	30	30	30	30	30
	Falls.	0	0	0	0	0	0	0	0	0	0
39000	Avg.	-0.064	-0.041	0.015	0.076	0.086	0.136	0.253	0.332	0.379	0.438
	Max	0.050	0.078	0.279	0.348	0.407	0.636	0.890	1.048	1.814	1.170
	Min	-0.280	-0.229	-0.216	-0.142	-0.051	-0.101	-0.050	-0.063	-0.050	0.081
	Sigma	0.079	0.069	0.079	0.094	0.105	0.126	0.176	0.200	0.340	0.218
	K-1	-1.050	-0.668	0.512	0.640	1.560	1.830	1.980	1.730	2.690	1.360
	N	30	30	30	30	30	30	30	30	30	30
	Falls.	0	0	0	0	0	0	0	0	Unstable	Unstable

TABLE I. TEMPERATURE LOAD MATRIX

TEST 70°C - 1/8 Watt Fail. Limit $\pm 5.0\%$ Page 8A of 30

RANGE	HOURS									
	5000									
	Avg.									
	Max									
	Min									
	Sigma									
	K-1									
	N									
	Fail									
	Avg.									
	Max									
	Min									
10 KG	Sigma									
	K-1									
	N									
	Fail									
	Avg.	0.685								
	Max	1.481								
	Min	0.324								
	Sigma	0.228								
	K-1	1.460								
	N	30								
	Fail	2								
	Avg.									
	Max									
	Min									
	Sigma									
	K-1									
	N									
	Fail									
	Avg.									
	Max									

Fail

TABLE I TEMPERATURE - LOAD MATRIX

TEST 70°C - 1/4 Watt

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS										
	50	100	250	500	750	1000	2000	3000	4000	5000	
100	Avg.	-0.016	0.003	0.000	-0.003	-0.003	-0.043	0.123	0.153	0.133	
	Max	0.299	0.299	0.398	0.199	0.299	0.299	0.900	0.902	1.300	
	Min	-0.495	-0.396	-0.495	-0.495	-0.495	-0.495	-0.396	-0.098	-0.495	
	Sigma	0.120	0.104	0.122	0.110	0.110	0.131	0.202	0.219	0.286	
	K-1	-1.900	-0.744	-1.030	-2.690	-2.240	-0.930	1.400	2.140	2.040	
	N	30	30	30	30	30	30	30	30	30	
1K0	Fails	0	0	0	0	0	0	0	0	0	
	Avg.	0.079	0.065	0.149	0.149	0.171	0.194	0.379	0.380	0.316	
	Max	1.234	0.345	1.234	1.382	1.343	1.531	2.143	2.054	2.024	
	Min	0.000	-0.048	0.000	-0.009	0.000	0.000	0.159	0.158	0.156	
	Sigma	0.217	0.072	-0.210	0.238	0.229	0.260	0.338	0.323	0.329	
	K-1	4.940	2.340	4.540	4.600	4.390	4.460	4.710	4.620	4.630	
10K0	N	30	30	30	30	30	30	30	30	30	
	Fails	0	0	0	0	0	0	0	0	0	
	Avg.	-0.015	0.085	0.561	0.520	0.411	0.570	1.020	1.260	1.490	
	Max	3.435	6.129	13.92	12.14	10.17	12.410	20.460	21.230	24.030	
	Min	-0.474	-0.569	-0.341	-0.332	-0.284	-0.284	-0.170	-0.507	0.000	
	Sigma	0.649	1.120	2.480	2.160	1.810	2.200	3.610	3.819	4.200	
39K0	K-1	4.980	5.080	5.180	5.170	5.150	5.170	5.180	4.780	5.120	
	N	30	30	30	30	30	30	30	30	30	
	Fails	0	1	1	1	1	1	1	1	1	
	Avg.	-0.137	-0.117	-0.072	-0.072	0.175	0.196	0.471	0.648	0.701	
	Max	0.228	0.228	0.339	0.738	0.989	1.090	1.894	3.778	2.321	
	Min	-1.079	-1.004	-0.451	-0.502	-0.276	-0.276	0.075	0.025	0.176	
39K0	Sigma	0.220	0.202	1.154	0.204	0.241	0.243	0.322	0.739	0.402	
	K-1	-2.550	-2.620	-0.774	0.516	1.480	1.610	2.490	2.870	1.960	
	N	30	30	30	30	30	30	30	30	30	
	Fails	0	0	0	0	0	0	0	0	0	
	Avg.	-0.137	-0.117	-0.072	-0.072	0.175	0.196	0.471	0.648	0.701	
	Max	0.228	0.228	0.339	0.738	0.989	1.090	1.894	3.778	2.321	

TABLE I TEMPERATURE LOAD MATRIX

TEST 70°C - 3/4 Watt

Fall. Limit $\pm 5.0\%$

Page 12 of 30

RANGE	HOURS										
	50	100	250	500	750	1000	2000	3000	4000	5000	
100	Avg.	-0.086	-0.090	-0.106	-0.089	-0.092	-0.065	1.490	2.190	5000	
	Max	0.000	0.000	0.201	0.300	0.300	0.616	7.150	8.850	10.214	
	Min	-0.400	-0.500	-0.600	-0.600	-0.600	-0.495	0.100	0.100	0.100	
	Sigma	0.095	0.110	0.170	0.183	0.204	0.232	1.310	1.600	1.880	
	K-1	-1.400	-1.970	-1.310	-0.953	-0.962	0.498	2.730	2.100	2.260	
	N	30	30	30	30	30	30	30	30	30	
100	Falls.	0	0	0	0	0	0	1	1	3	
	Avg.	-0.135	-0.204	-0.192	-0.256	-0.409	-0.276	0.252	0.129	0.044	
	Max	0.176	0.097	0.389	0.535	0.618	0.477	5.449	100.00	1.224	
	Min	-0.447	-0.489	-0.587	-0.743	-1.629	-0.880	-0.511	-0.2422	-0.503	
	Sigma	0.147	0.147	0.207	0.248	0.507	0.279	1.020	0.372	0.372	
	K-1	-0.159	-0.225	0.510	0.766	-0.305	0.381	4.320	1.070	1.070	
1000	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	0	0	1	1	1	
	Avg.	-0.152	-0.182	-0.104	-0.128	-0.073	0.143	2.760	2.890	3.480	
	Max	0.272	0.070	0.202	0.477	0.552	1.119	7.027	7.886	9.119	
	Min	-0.425	-0.425	-0.260	-0.320	-0.519	-0.480	0.432	0.255	0.550	
	Sigma	0.120	0.108	0.114	0.132	0.268	0.419	1.420	1.780	1.850	
3900	K-1	1.070	0.086	0.483	0.115	0.562	0.463	0.938	1.050	1.180	
	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	0	0	3	3	4	
	Avg.	-0.097	-0.209	-0.216	-0.227	-0.192	-0.011	2.810	4.400	2.420	
	Max	0.220	0.322	0.250	1.243	1.704	2.662	28.887	64.115	10.442	
	Min	-0.658	-0.681	-0.593	-0.709	-0.784	-0.633	0.372	-0.381	0.524	
3900	Sigma	0.202	0.226	0.211	0.352	0.459	0.710	5.130	11.290	2.020	
	K-1	-0.517	-0.207	0.046	2.340	2.450	2.320	4.510	4.960	2.490	
	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	0	0	4	4	4	
	Avg.	-0.097	-0.209	-0.216	-0.227	-0.192	-0.011	2.810	4.400	2.420	
	Max	0.220	0.322	0.250	1.243	1.704	2.662	28.887	64.115	10.442	
	Min	-0.658	-0.681	-0.593	-0.709	-0.784	-0.633	0.372	-0.381	0.524	
	Sigma	0.202	0.226	0.211	0.352	0.459	0.710	5.130	11.290	2.020	
	K-1	-0.517	-0.207	0.046	2.340	2.450	2.320	4.510	4.960	2.490	
	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	0	0	4	4	4	

TABLE I. TEMPERATURE LOAD MATRIX

TEST

35°C No Load

Full. Limit $\pm 5.0\%$

[illegible]

TABLE I TEMPERATURE LOAD MATRIX

TEST 85°C 0 - 1/4 W

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS									
	6000									
10 Ω	Avg.	0.155								
	Max	1.892								
	Min	-0.195								
	Sigma	0.299								
	K-1	2.620								
	N	100								
	Falls.	0								
1 K Ω	Avg.	0.288								
	Max	0.678								
	Min	0.000								
	Sigma	0.132								
	K-1	0.666								
	N	100								
	Falls.	0								
10 K Ω	Avg.	0.367								
	Max	1.216								
	Min	-3.595								
	Sigma	0.508								
	K-1	-4.710								
	N	100								
	Falls.	0								
39 K Ω	Avg.	0.338								
	Max	1.597								
	Min	-1.817								
	Sigma	0.340								
	K-1	-1.690								
	N	100								
	Falls.	0								

TABLE I TEMPERATURE LOAD MATRIX

TEST 85°C - 1/2 hr

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS
Avg.	6000
Max	
Min	
Sigma	
K-1	
N	
Falls	
Avg.	
Max	
Min	
Sigma	
K-1	
N	
Falls	
Avg.	2,310
Max	38.05
Min	-0.058
Sigma	6,690
K-1	5,050
N	30
Falls	1
Avg.	1,630
Max	4,386
Min	0,320
Sigma	0,912
K-1	1,170
N	30
Falls	0

TABLE I TEMPERATURE - LOAD MATRIX

TEST 85°C 3/4 Watt

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS										
	50	100	250	500	750	1000	2000	3000	4000	5000	
100	Avg.	-0.108	-0.168	-0.165	-0.151	-0.016	0.077	1.270	2.920	3.890	
	Max	0.298	0.199	0.199	0.607	1.215	2.502	15.02	18.200	20.000	
	Min	-0.594	-0.600	-0.600	-0.700	-0.600	-0.600	-0.099	0.000	0.800	
	Sigma	0.190	0.216	0.218	0.266	0.369	0.537	2.900	3.650	4.070	
	K-1	-0.920	-0.966	-0.974	0.001	1.510	3.220	3.740	2.740	2.420	
	N	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	0	0	0	4	6	7	
1K0	Avg.	-0.209	-0.409	-0.426	-0.317	-0.202	-0.121	-0.029	0.081	0.352	
	Max	0.048	0.380	0.702	0.937	1.034	1.181	1.464	1.767	2.206	
	Min	-0.744	-1.107	-1.234	-1.038	-0.582	-0.473	-0.380	-0.331	-0.176	
	Sigma	0.131	0.255	0.346	0.370	0.317	0.327	0.406	0.459	0.519	
	K-1	-1.800	0.452	0.736	0.995	2.060	2.230	1.990	1.970	2.180	
	N	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	0	0	0	0	0	0	
10K0	Avg.	-0.349	-0.394	-0.553	0.107	0.387	0.973	2.330	3.160	5.090	
	Max	-0.011	0.032	0.211	11.93	6.11	11.014	11.894	13.466	58.050	
	Min	-1.141	-1.211	-1.299	-0.878	-0.512	-0.416	0.173	0.000	0.349	
	Sigma	0.229	0.242	0.326	2.230	1.330	2.110	2.440	3.190	1.010	
	K-1	-1.660	-1.350	-0.035	4.930	3.740	3.640	2.210	1.880	4.660	
	N	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	1	1	1	3	6	7	
39K	Avg.	-0.205	-0.308	-0.465	-0.327	0.146	1.280	2.563	3.150	4.920	
	Max	2.092	1.990	1.812	1.891	2.783	20.050	>100.00	12.399	44.376	
	Min	-0.899	-0.951	-1.333	-0.891	-0.840	-0.401	0.794	0.814	0.977	
	Sigma	0.494	0.499	0.513	0.622	0.949	3.670	5.592	2.560	7.930	
	K-1	3.120	3.070	2.790	2.250	1.650	4.440	5.190	2.050	4.240	
	N	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	0	0	1	5	5	7	

TABLE I TEMPERATURE - LOAD MATRIX

TEST 125°C - NO LOAD

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS -										
	50	100	250	500	750	1000	2000	3000	4000	5000	
100	Avg.	No	0.406	0.373	0.396	-0.325	0.658	0.046	0.516	-0.662	
	Max	No	0.909	0.909	1.215	0.103	1.507	1.395	2.093	2.193	
	Min		-0.099	-0.199	-0.199	-0.700	-0.102	-0.203	0.000	-19.620	
	Sigma		0.315	0.314	0.360	0.183	0.479	0.280	0.440	3.550	
	K-1		0.126	-0.017	0.140	0.486	0.016	3.630	1.890	-5.040	
	N		30	30	30	30	30	30	30	30	
1K0	Fails.		0	0	0	0	0	0	0	1	
	Avg.		0.055	0.062	0.041	0.046	0.080	0.070	0.133	0.116	
	Max	No	0.208	0.308	0.298	0.237	0.397	0.387	0.317	0.447	
	Min	No	-0.069	-0.118	-0.149	-0.149	-0.179	-0.249	-0.209	0.259	
	Sigma		0.082	0.122	0.128	0.130	0.151	0.139	0.136	0.119	
	K-1		0.307	0.335	0.291	0.213	0.054	-0.181	-0.397	-0.615	
10K0	N		30	30	30	30	30	30	30	30	
	Fails.		0	0	0	0	0	0	0	0	
	Avg.		-0.018	-0.007	0.024	0.104	0.107	0.153	0.306	0.474	
	Max	No	0.488	0.603	0.708	1.005	1.255	1.417	1.628	1.916	
	Min	No	-0.163	-0.200	-0.220	-0.115	-0.231	-0.316	-0.299	-0.299	
	Sigma		0.122	0.168	0.184	0.239	0.318	0.362	0.386	0.440	
39K0	K-1		2.280	2.120	2.420	2.660	2.370	1.890	1.530	1.330	
	N		30	30	30	30	30	30	30	30	
	Fails.		0	0	0	0	0	0	0	0	
	Avg.		-0.004	-0.040	-0.032	-0.026	-0.079	-0.067	0.008	0.106	
	Max		0.319	0.253	0.163	0.214	0.266	0.312	0.400	0.664	
	Min		-0.107	-0.233	-0.307	-0.282	-0.939	-1.015	-0.406	-0.461	
39K0	Sigma		0.069	0.082	0.076	0.089	0.190	0.233	0.182	0.206	
	K-1		3.380	1.150	-0.620	-2.900	-2.890	-2.130	0.068	0.003	
	N		30	30	30	30	30	30	30	30	
	Fails.		0	0	0	0	0	0	0	0	
	Avg.		-0.004	-0.040	-0.032	-0.026	-0.079	-0.067	0.008	0.106	
	Max		0.319	0.253	0.163	0.214	0.266	0.312	0.400	0.664	
39K0	Min		-0.107	-0.233	-0.307	-0.282	-0.939	-1.015	-0.406	-0.461	
	Sigma		0.069	0.082	0.076	0.089	0.190	0.233	0.182	0.206	
	K-1		3.380	1.150	-0.620	-2.900	-2.890	-2.130	0.068	0.003	
	N		30	30	30	30	30	30	30	30	
	Fails.		0	0	0	0	0	0	0	0	
	Avg.		-0.004	-0.040	-0.032	-0.026	-0.079	-0.067	0.008	0.106	
39K0	Max		0.319	0.253	0.163	0.214	0.266	0.312	0.400	0.664	
	Min		-0.107	-0.233	-0.307	-0.282	-0.939	-1.015	-0.406	-0.461	
	Sigma		0.069	0.082	0.076	0.089	0.190	0.233	0.182	0.206	
	K-1		3.380	1.150	-0.620	-2.900	-2.890	-2.130	0.068	0.003	
	N		30	30	30	30	30	30	30	30	
	Fails.		0	0	0	0	0	0	0	0	

TABLE I TEMPERATURE - LOAD MATRIX

TEST 125°C - 1/8 Watt Fall. Limit $\pm 5.0\%$ Page 20 of 30

RANGE	HOURS										
	50	100	250	500	750	1000	2000	3000	4000	5000	
100	Avg.	-0.105	-0.177	-0.200	-0.197	-0.328	-0.279	-0.309	-0.299	-0.130	
	Max	0.000	0.000	0.295	0.493	0.000	0.295	0.099	0.198	0.498	
	Min	-0.490	-0.679	0.970	-1.067	-1.380	-1.359	-1.359	-1.553	-1.456	
	Sigma	0.150	0.195	0.241	0.266	0.325	0.317	0.289	0.332	0.358	
	K-1	-1.670	-1.230	-1.100	-0.837	-1.490	-1.210	-1.570	-1.900	-1.590	
	N	30	30	30	30	30	30	30	30	30	
1K0	Falls	0	0	0	0	0	0	0	0	0	
	Avg.	0.110	-0.177	-0.199	-0.199	-0.199	-0.188	-0.147	-0.094	0.114	
	Max	0.000	0.000	0.000	0.000	0.038	0.204	0.389	0.408	0.602	
	Min	-0.287	-0.287	-0.354	-0.354	-0.387	-0.574	-0.641	-0.574	-0.268	
	Sigma	0.072	0.072	0.086	0.086	0.119	0.192	0.206	0.193	0.187	
	K-1	0.781	0.781	0.499	0.499	0.765	0.398	0.184	0.162	0.441	
10K0	N	30	30	30	30	30	30	30	30	30	
	Falls	0	0	0	0	0	0	0	0	0	
	Avg.	-0.265	-0.265	0.032	0.032	-0.129	+0.097	0.228	0.509	0.536	
	Max	0.918	0.918	1.221	1.221	0.918	1.311	1.412	1.776	2.058	
	Min	-0.873	-0.873	-0.383	-0.383	-0.582	-0.488	-0.379	0.000	-0.038	
	Sigma	0.349	0.349	0.275	0.275	0.264	0.356	0.358	0.406	0.509	
39K0	K-1	1.150	1.150	2.580	2.580	1.860	1.110	1.250	1.320	1.560	
	N	30	30	30	30	30	30	30	30	30	
	Falls	0	0	0	0	0	0	0	0	0	
	Avg.	-0.036	-0.042	-0.065	-0.065	-0.127	-0.091	-0.045	0.119	0.144	
	Max	2.865	2.104	2.046	1.914	1.861	1.313	1.015	1.015	1.089	
	Min	-0.313	-1.509	-1.509	-2.120	-2.247	-2.980	-3.214	-3.265	-3.461	
39K0	Sigma	0.531	0.488	0.555	0.536	0.549	0.612	0.643	0.689	0.730	
	K-1	4.990	3.150	1.680	-0.210	-0.345	-1.180	-3.780	-3.790	-3.850	
	N	30	30	30	30	30	30	30	30	30	
	Falls	0	0	0	0	0	0	0	0	0	
	Avg.	0.039	0.039	0.042	0.042	0.127	0.091	0.045	0.119	0.144	
	Max	2.865	2.104	2.046	1.914	1.861	1.313	1.015	1.015	1.089	
39K0	Min	-0.313	-1.509	-1.509	-2.120	-2.247	-2.980	-3.214	-3.265	-3.461	
	Sigma	0.531	0.488	0.555	0.536	0.549	0.612	0.643	0.689	0.730	
	K-1	4.990	3.150	1.680	-0.210	-0.345	-1.180	-3.780	-3.790	-3.850	
	N	30	30	30	30	30	30	30	30	30	
	Falls	0	0	0	0	0	0	0	0	0	
	Avg.	0.039	0.039	0.042	0.042	0.127	0.091	0.045	0.119	0.144	

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Full. Limit $\pm 5.0\%$

TABLE I TEMPERATURE - LOAD MATRIX

TEST 125°C - 1/2 Watt Fall. Limit $\pm 5.0\%$

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RANGE	HOURS										
	50	100	250	500	750	1000	2000	3000	4000	5000	
100	Avg.	-0.128	-0.174	-0.309	-0.263	-0.138	-0.039	1.180	1.490	1.660	
	Max	0.146	0.196	0.999	0.294	0.981	0.981	2.994	3.925	4.416	
	Min	-0.583	-0.699	-0.999	-1.098	-0.626	-0.874	0.388	0.588	0.691	
	Sigma	0.190	0.200	0.262	0.314	0.537	0.428	0.623	0.768	0.843	
	K-1	-1.310	-0.787	-0.921	-0.873	0.767	0.125	1.140	1.220	1.410	
	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	0	0	0	0	0	
1K0	Avg.			-0.634	-0.487	-0.250	-0.149	0.064	0.092	0.372	
	Max			0.154	0.038	0.202	0.385	0.578	0.521	0.889	
	Min			-1.016	-1.114	-0.892	-0.650	-0.231	-0.163	0.067	
	Sigma			0.224	0.239	0.263	0.199	0.210	0.212	0.219	
	K-1			0.539	-0.486	-0.488	0.224	0.988	1.080	0.836	
	N			30	30	30	30	30	30	30	
	Falls.			0	0	0	0	0	0	0	
10K0	Avg.	-0.316	-0.665	-0.511	-0.273	0.655	0.710	2.530	2.860	2.960	
	Max	2.137	0.000	2.672	2.996	10.000	3.273	6.511	6.758	7.063	
	Min	-1.012	-1.927	-1.324	-0.917	-0.526	-0.480	0.686	0.784	0.833	
	Sigma	0.485	0.344	0.659	0.701	2.320	0.896	1.200	1.260	1.280	
	K-1	4.180	-1.650	3.680	3.390	4.320	0.814	0.983	0.753	0.848	
	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	1	2	2	2	2	
39K0	Avg.	-0.254	-0.396	-0.312	-0.078	0.250	0.623	1.300	1.420	1.280	
	Max	2.194	1.765	2.371	2.850	3.254	3.685	6.735	7.013	6.634	
	Min	-1.040	-1.141	-1.141	-1.116	-1.015	-0.762	0.280	-0.253	-0.402	
	Sigma	0.480	0.435	0.543	0.642	0.726	0.837	1.330	1.610	1.340	
	K-1	4.250	3.880	3.910	3.080	2.000	1.940	2.590	2.120	2.440	
	N	30	30	30	30	30	30	30	30	30	
	Falls.	0	0	0	0	0	1	1	2	2	

TABLE I TEMPERATURE - LOAD MATRIX

TESTE 125°C - 3/4 Watt

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS											
	50	100	250	500	750	1000	2000	3000	4000	5000		
100	Avg.	-0.612	-0.526	-0.388	3.230	4.010	4.710	5.810	6.530	7.030	5000	
	Max	2.660	3.645	4.433	7.262	11.209	11.504	12.757	14.720	15.897	19.842	
	Min	-1.883	-1.793	-1.793	0.891	1.188	1.386	1.881	2.079	2.178	2.475	
	Sigma	0.719	0.869	1.010	1.800	2.320	2.460	2.590	2.910	3.200	3.940	
	K-1	2.840	3.490	3.370	0.567	1.150	0.857	0.565	0.762	0.773	1.290	
	N	30	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	7	11	12	18	21	24		
1K0	Avg.	<i>Pa</i>	<i>Pa</i>	-0.340	-0.096	0.033	0.097	0.278	0.497	0.689	1.140	
	Max			0.133	0.477	0.701	0.877	1.286	1.871	2.358	2.805	
	Min			-0.990	-0.414	-0.318	-0.384	-0.125	0.009	0.134	0.427	
	Sigma			0.282	0.211	0.240	0.262	0.322	0.438	0.514	0.533	
	K-1			-0.432	0.623	0.714	0.752	1.240	1.660	1.800	1.670	
	N			30	30	30	30	30	30	30	30	
	Fails.			0	0	0	0	0	0	0	0	
10K0	Avg.	-0.973	-0.912	-0.224	1.730	2.020	3.270	3.790	8.760	-4.380	4.420	
	Max	0.197	0.296	3.612	8.460	9.316	9.981	10.580	143.9	11.255	11.379	
	Min	-2.134	-1.930	-1.603	-0.521	0.354	0.255	0.551	0.846	0.974	0.885	
	Sigma	0.379	0.416	1.060	1.260	2.000	2.030	2.150	2.510	2.220	2.210	
	K-1	-0.257	0.373	1.880	2.140	1.640	1.790	1.640	5.140	1.600	1.510	
	N	30	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	3	4	4	5	7	9	10	
39K0	Avg.	-0.816	-0.745	-0.040	0.807	1.330	1.300	1.560	1.770	1.970	1.890	
	Max	0.318	1.222	2.143	3.579	4.757	8.773	9.721	9.845	10.344	10.200	
	Min	-2.516	-2.615	-2.541	-1.554	0.096	-0.814	-0.320	-0.197	-0.148	0.289	
	Sigma	0.414	0.505	0.340	1.000	1.160	1.780	1.940	1.940	1.980	1.970	
	K-1	-1.630	0.279	0.184	0.764	1.370	2.590	2.650	2.560	2.640	2.620	
	N	30	30	30	30	30	30	30	30	30	30	
	Fails.	0	0	0	0	0	1	1	1	3	3	

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[illegible]

TEST 150°C - 1/8 W

Fail. Lin It $\pm 5.0\%$

[illegible]

TABLE I TEMPERATURE LOAD MATRIX

TEST 150°C 3/8 Watt

Fail. Limit $\pm 5.0\%$

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RANGE	HOURS											
	50	100	250	500	750	1000	2000	3000	4000	5000		
10 Ω	Avg.	-0.131	-0.332	-0.272	-0.292	-0.170	0.119	0.984	1.080	1.230		
	Max	0.397	0.098	0.297	0.397	1.191	1.191	1.697	2.184	2.184		
	Min	-0.679	-0.970	-0.990	-0.970	-1.067	-1.067	0.298	0.298	0.298		
	Sigma	0.207	0.266	0.287	0.309	0.402	0.404	0.354	0.447	0.475		
	K-1	-0.509	-0.754	-0.844	-0.382	0.694	0.164	0.551	0.541	0.227		
	N	30	30	30	30	30	30	30	30	30		
	Fails.	0	0	0	0	0	0	0	0	0		
1K Ω	Avg.	-0.126	-0.332	-0.048	0.015	0.036	0.172	0.762	0.954	1.130		
	Max	0.247	0.000	0.288	0.332	0.573	0.955	1.977	2.015	2.101		
	Min	-0.656	-0.946	-0.528	-0.380	-0.526	-2.437	0.142	0.191	0.393		
	Sigma	0.159	0.201	0.200	0.190	0.270	0.551	0.355	0.411	0.474		
	K-1	-0.742	-1.030	-0.522	-0.035	3.120	-3.370	0.991	0.291	0.179		
	N	30	30	30	30	30	30	30	30	30		
	Fails.	0	0	0	0	0	0	0	0	0		
10K Ω	Avg.	-0.357	-0.496	-0.484	0.336	0.833	1.450	2.160	2.660	2.760		
	Max	4.386	5.273	4.288	6.140	5.653	7.320	10.137	11.112	10.956		
	Min	-0.965	-1.341	-1.274	-0.686	-0.182	-0.182	0.009	0.394	0.423		
	Sigma	0.921	1.120	0.987	1.170	1.050	1.350	1.780	1.900	1.860		
	K-1	4.520	4.430	3.760	3.960	3.100	2.680	2.920	2.890	2.770		
	N	30	30	30	30	30	30	30	30	30		
	Fails.	0	1	1	1	1	1	2	2	2		
39K Ω	Avg.	-0.338	-0.440	-0.481	0.103	0.382	0.823	1.480	1.810	1.740		
	Max	1.454	1.594	1.772	2.573	3.204	4.113	7.139	6.911	6.303		
	Min	-2.467	-2.742	-2.987	-2.597	-2.597	-2.597	-2.077	-1.896	-1.860		
	Sigma	0.674	0.709	0.755	0.904	1.000	1.250	1.560	1.580	1.550		
	K-1	-0.465	0.307	0.127	0.442	0.475	1.160	1.490	1.030	0.950		
	N	30	30	30	30	30	30	30	30	30		
	Fails.	0	0	0	0	0	0	1	1	1		

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TEST

Fail. Limit $\pm 5.0\%$

Page 1 of 30

[illegible]

Fall. Limit $\pm 5.0\%$

TEST 25°C - 1/4 Watt

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[illegible]

TABLE II TEMPERATURE - LOAD MATRIX

TEST
70°C - 1/8 Watt

Fall. Limit $\pm 5.0\%$

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[illegible]

TEST	85°C No Load	Fall. Limit $\pm 5.0\%$
1. Initial	100.0	
2. After 1 hr	100.0	
3. After 2 hr	100.0	
4. After 3 hr	100.0	
5. After 4 hr	100.0	
6. After 5 hr	100.0	
7. After 6 hr	100.0	
8. After 7 hr	100.0	
9. After 8 hr	100.0	
10. After 9 hr	100.0	
11. After 10 hr	100.0	
12. After 11 hr	100.0	
13. After 12 hr	100.0	
14. After 13 hr	100.0	
15. After 14 hr	100.0	
16. After 15 hr	100.0	
17. After 16 hr	100.0	
18. After 17 hr	100.0	
19. After 18 hr	100.0	
20. After 19 hr	100.0	
21. After 20 hr	100.0	
22. After 21 hr	100.0	
23. After 22 hr	100.0	
24. After 23 hr	100.0	
25. After 24 hr	100.0	
26. After 25 hr	100.0	
27. After 26 hr	100.0	
28. After 27 hr	100.0	
29. After 28 hr	100.0	
30. After 29 hr	100.0	
31. After 30 hr	100.0	
32. After 31 hr	100.0	
33. After 32 hr	100.0	
34. After 33 hr	100.0	
35. After 34 hr	100.0	
36. After 35 hr	100.0	
37. After 36 hr	100.0	
38. After 37 hr	100.0	
39. After 38 hr	100.0	
40. After 39 hr	100.0	
41. After 40 hr	100.0	
42. After 41 hr	100.0	
43. After 42 hr	100.0	
44. After 43 hr	100.0	
45. After 44 hr	100.0	
46. After 45 hr	100.0	
47. After 46 hr	100.0	
48. After 47 hr	100.0	
49. After 48 hr	100.0	
50. After 49 hr	100.0	
51. After 50 hr	100.0	
52. After 51 hr	100.0	
53. After 52 hr	100.0	
54. After 53 hr	100.0	
55. After 54 hr	100.0	
56. After 55 hr	100.0	
57. After 56 hr	100.0	
58. After 57 hr	100.0	
59. After 58 hr	100.0	
60. After 59 hr	100.0	
61. After 60 hr	100.0	
62. After 61 hr	100.0	
63. After 62 hr	100.0	
64. After 63 hr	100.0	
65. After 64 hr	100.0	
66. After 65 hr	100.0	
67. After 66 hr	100.0	
68. After 67 hr	100.0	
69. After 68 hr	100.0	
70. After 69 hr	100.0	
71. After 70 hr	100.0	
72. After 71 hr	100.0	
73. After 72 hr	100.0	
74. After 73 hr	100.0	
75. After 74 hr	100.0	
76. After 75 hr	100.0	
77. After 76 hr	100.0	
78. After 77 hr	100.0	
79. After 78 hr	100.0	
80. After 79 hr	100.0	
81. After 80 hr	100.0	
82. After 81 hr	100.0	
83. After 82 hr	100.0	
84. After 83 hr	100.0	
85. After 84 hr	100.0	
86. After 85 hr	100.0	
87. After 86 hr	100.0	
88. After 87 hr	100.0	
89. After 88 hr	100.0	
90. After 89 hr	100.0	
91. After 90 hr	100.0	
92. After 91 hr	100.0	
93. After 92 hr	100.0	
94. After 93 hr	100.0	
95. After 94 hr	100.0	
96. After 95 hr	100.0	
97. After 96 hr	100.0	
98. After 97 hr	100.0	
99. After 98 hr	100.0	
100. After 99 hr	100.0	
101. After 100 hr	100.0	
102. After 101 hr	100.0	
103. After 102 hr	100.0	
104. After 103 hr	100.0	
105. After 104 hr	100.0	
106. After 105 hr	100.0	
107. After 106 hr	100.0	
108. After 107 hr	100.0	
109. After 108 hr	100.0	

[illegible]

TEST 85.C 178-W42

Fe³⁺. Limit $\pm 5.0\%$ [illegible]

Fall. Limit 45.0%

TEST
85°C - 1/4 Watt

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[illegible]

TEST 85°C - 1/2 Watt

Fail. Limit $\pm 5.0\%$

[illegible]

01030

[illegible]

Fail. Limit $\pm 5.0\%$

125°C - 3/8 Watt

TEST I

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[illegible]

TTLST 150°C - No Load Fall. Limit $\pm 5.0\%$

[illegible]

Fall. Limit $\pm 5.0\%$

150-C - 18 W

1971

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[illegible]

Fail. Limit $\pm 5, 0\%$

150°C - 180 W

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[illegible]

Fail. Limit $\pm 5.0\%$

150°C - 1/2 W

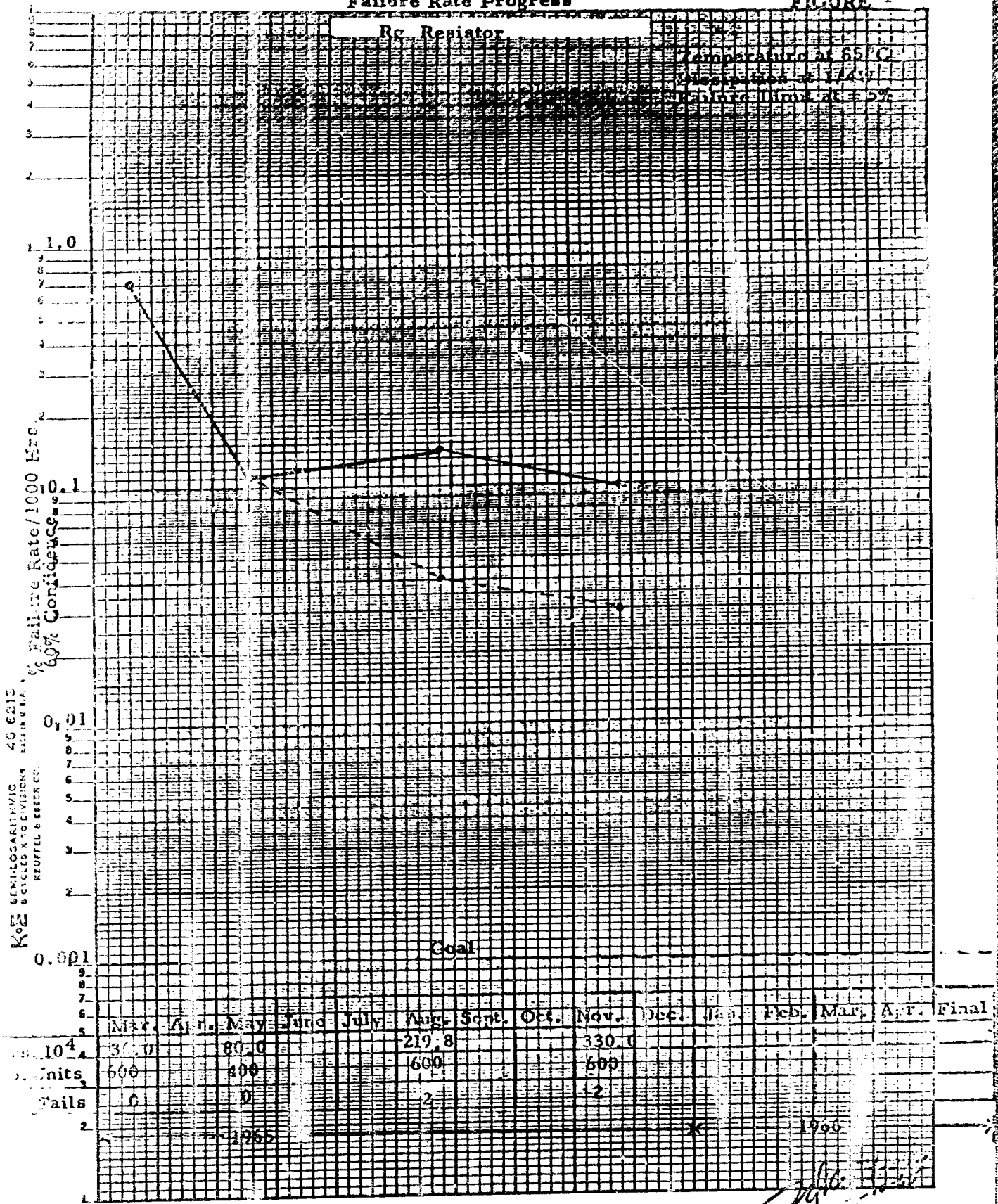
TEST

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[illegible]

Failure Rate Progress

FIGURE 1



RETRIEVAL DISTRIBUTION

Fig. 2

CELL WIDTH 0.100 S

05E-1/4 WATT - 10³ 5000 Hcs

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00000) I

-0006 (00001) IX

-0005 (00000) I

-0004 (00001) IX

-0003 (00001) IX

-0002 (00002) IXX

-0001 (00004) IXXXX

0000 (00020) IXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0001 (00020) IXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0002 (00018) IXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0003 (00012) IXXXXXXXXXXXXXXXXXXXX

0004 (00000) I

0005 (00003) IXXX

0006 (00002) IXX

0007 (00003) IXXX

0008 (00002) IXX

0009 (00000) I

0010 (00001) IX

0011 (00000) I

0012 (00000) I

0013 (00000) I

0014 (00000) I

0015 (00001) IX

0016 (00000) I

0017 (00000) I

0018 (00000) I

0019 (00000) I

0020 (00000) I

0021 (00000) I

0022 (00000) I

0023 (00000) I

0024 (00003) I

0025 (00000) I

0026 (00000) I

0027 (00000) I

0028 (00000) I

0029 (00000) I

0030 (00000) I

0031 (00000) I

0032 (00000) I

0033 (00000) I

0034 (00000) I

0035 (00000) I

0036 (00000) I

0037 (00000) I

0038 (00000) I

0039 (00000) I

0040 (00000) I

0041 (00000) I

0042 (00000) I

0043 (00000) I

0044 (00000) I

0045 (00000) I

0046 (00000) I

0047 (00000) I

0048 (00000) I

CALCULATIONS/SUMMARY

NUMBER 0.10000-03

MEAN 0.19362-00

VARIANCE 0.30210-00

STD. DEV. 0.54964-00

SKEWNESS 0.60253-01

KURTOSIS 0.50917-02

RETRIEVAL DISTRIBUTION

FIG 3

CELL WIDTH 0.100 ± 852-1/4 WATT-10⁵-600 Hertz

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00000) 1

-0002 (00007) IXXXXXXXX

-0001 (00004) IXXXX

0000 (00035) IXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0001 (00016) IXXXXXXXXXXXXXXXXXXXX

0002 (00017) IXXXXXXXXXXXXXXXXXXXX

0003 (00004) IXXXX

0004 (00000) 1

0005 (00005) IXXXXX

0006 (00004) IXXXX

0007 (00001) IX

0008 (00005) IXXXXX

0009 (00000) 1

0010 (00000) 1

0011 (00001) IX

0012 (00000) 1

0013 (00000) 1

0014 (00000) 1

0015 (00000) 1

0016 (00000) 1

0017 (00000) 1

0018 (00000) 1

0019 (00001) IX

OVER (00000) 1

CALCULATIONS/SUMMARY

NUMBER 0.10000-03

MEAN 0.15577-00

VARIANCE 0.09640-01

STD. DEV. 0.29940-00

SKEWNESS 0.24213-01

KURTOSIS 0.13230-02

RETRIEVAL DISTRIBUTION

FIG. 4

CELL WIDTH 0.100 \times 85 $^{\circ}$ - 1/4 WATT - 1K $^{\circ}$ 5000 HZ

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00000) 1

0000 (00000)	1
0001 (00004)	XXXX
0002 (00016)	XXXXXXXXXXXXXXXXXXXX
0003 (00039)	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
0004 (00025)	XXXXXXXXXXXXXXXXXXXXXXXXXXXX
0005 (00009)	XXXXXXXXXX
0006 (00005)	XXXXXX
0007 (00002)	XXX

OVER (00000) 1

CALCULATIONS/SUMMARY

NUMBER	0.10000-03
MEAN	0.29483-00
VARIANCE	0.16192-01
STD. DEV.	0.12709-00
SKEWNESS	0.60204-00
KURTOSIS	0.35510-01

RETRIEVAL DISTRIBUTION

FIG 8

CELL WIDTH 0.100 X 850 - 1/4 WATT - LK² - 6000 Hz

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

OVER (00000) 1

0000	(00001)	IX
0001	(00004)	XXXX
0002	(00019)	XXXXXXXXXXXXXXXXXXXX
0003	(00042)	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX
0004	(00026)	XXXXXXXXXXXXXXXXXXXX
0005	(00006)	XXXXXX
0006	(00005)	XXXXXX
0007	(00003)	XXXX

OVER (00000) 1

CALCULATIONS/SUMMARY

NUMBER	0.10000-03
MEAN	0.28017-00
VARIANCE	0.17671-01
STD. DEV.	0.13293-00
SKEWNESS	0.66661-00
KURTOSIS	0.36023-01

RETRIEVAL DISTRIBUTION

FIG. 6

CELL WIDTH 0.100 % 85°C - 1/2 WATT - 10K² - 5000 HZ

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00000) I

-0013 (00001) IX

-0012 (00000) I

-0011 (00001) IX

-0010 (00000) I

-0009 (00000) I

-0008 (00000) I

-0007 (00000) I

-0006 (00000) I

-0005 (00000) I

-0004 (00001) IX

-0003 (00000) I

-0002 (00002) IXX

-0001 (00002) IXX

0000 (00001) IX

0001 (00005) IXXXXX

0002 (00009) IXXXXXXXXXX

0003 (00017) IXXXXXXXXXXXXXXXXXX

0004 (00012) IXXXXXXXXXXXXXX

0005 (00014) IXXXXXXXXXXXXXXXXXX

0006 (00012) IXXXXXXXXXXXXXX

0007 (00008) IXXXXXXXXXX

0008 (00007) IXXXXXXX

0009 (00003) IXXX

0010 (00003) IXXX

0011 (00001) IX

0012 (00001) IX

OVER (00000) I

CALCULATIONS/SUMMARY

MUNSEN 0.10690-03

MEAN 0.30471-00

VARIANCE 0.12201-00

STD. DEV. 0.34930-00

SKEWNESS -0.15787-01

KURTOSIS 0.91320-01

RETRIEVAL DISTRIBUTION

FIG. 7

CELL WIDTH 0.100 X 852 -1/4 WATT- 10K² 6000 HZES.

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00000) 1

-0036 (00001) IX

-0035 (00000) I

-0034 (00000) I

-0033 (00000) I

-0032 (00000) I

-0031 (00000) I

-0030 (00000) I

-0029 (00000) I

-0028 (00000) I

-0027 (00000) I

-0026 (00000) I

-0025 (00000) I

-0024 (00000) I

-0023 (00000) I

-0022 (00000) I

-0021 (00000) I

-0020 (00000) I

-0019 (00000) I

-0018 (00000) I

-0017 (00000) I

-0016 (00000) I

-0015 (00000) I

-0014 (00000) I

-0013 (00000) I

-0012 (00000) I

-0011 (00000) I

-0010 (00001) IX

-0009 (00000) I

-0008 (00000) I

-0007 (00000) I

-0006 (00000) I

-0005 (00000) I

-0004 (00001) IX

-0003 (00000) I

-0002 (00001) IX

-0001 (00003) IXXX

0000 (00000) I

0001 (00004) IXXXX

0002 (00012) IXXXXXXXXXXXXX

0003 (00016) IXXXXXXXXXXXXXXXXX

0004 (00013) IXXXXXXXXXXXXX

0005 (00013) IXXXXXXXXXXXXX

0006 (00017) IXXXXXXXXXXXXXXXXX

0007 (00005) IXXXXX

0008 (00005) IXXXXX

0009 (00002) IXX

0010 (00000) I

0011 (00003) IXXX

0012 (00001) IX

0013 (00001) IX

0014 (00001) IX

OVER (00000) 1

CALCULATIONS/SUMMARY

NUMBER 0.10000-03

MEAN 0.36742-00

VARIANCE 0.25822-00

STD. DEV. 0.50816-00

SKEWNESS -0.47156-01

KURTOSIS 0.37914-02

RETRIEVAL DISTRIBUTION

F.G. 8

CELL WIDTH 0.100 S 85% 1/4 WATT - 39 Hz. 5000 Hz

CELL NO. 0 10 20 30 40 50

OVER (000000) I

0018 (000001) IX

0017 (000000) I

0016 (000000) I

0015 (000000) I

0014 (000000) I

0013 (000000) I

0012 (000000) I

0011 (000000) I

0010 (000000) I

0009 (000000) I

0008 (000000) I

0007 (000000) I

0006 (000000) I

0005 (000000) I

0004 (000000) I

0003 (000001) IX

0002 (000000) I

0001 (000000) I

0000 (000001) IX

0001 (000100) IXXXXXXXXXX

0002 (000100) IXXXXXXXXXXXXXXXXXX

0003 (000200) IXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0004 (000100) IXXXXXXXXXXXX

0005 (000100) IXXXXXXXXXXXXXXXX

0006 (000000) IXXXXXXXXXX

0007 (000000) IXXXX

0008 (000001) IX

0009 (000003) IXXX

0010 (000001) IX

0011 (000002) IXX

0012 (000000) I

0013 (000000) I

0014 (000000) I

0015 (000000) I

0016 (000001) IX

0017 (000000) I

0018 (000000) I

0019 (000000) I

0020 (000001) IX

OVER (000000) I

CALCULATIONS/SUMMARY

NUMBER 0.10000.03

MEAN 0.33655.00

VARIANCE 0.13640.00

STD. DEV. 0.36933.00

SKEWNESS -0.58424.00

KURTOSIS 0.16167.02

RETRIEVAL DISTRIBUTION

FIG. 9

CELL WIDTH 0.100 % 352 - 1/4 WATT - 59 kHz Goodhart.

CELL NO.	0	10	20	30	40	50
.....

OVER (000000) I

00019	(000001)	I
00018	(000000)	I
00017	(000000)	I
00016	(000000)	I
00015	(000000)	I
00014	(000000)	I
00013	(000000)	I
00012	(000000)	I
00011	(000000)	I
00010	(000000)	I
00009	(000000)	I
00008	(000000)	I
00007	(000000)	I
00006	(000000)	I
00005	(000000)	I
00004	(000000)	I
00003	(000000)	I
00002	(000001)	IX
00001	(000000)	I
00000	(000000)	I
00001	(000012)	XXXXXXXXXXXXXX
00002	(000010)	XXXXXXXXXXXXXX
00003	(000029)	XXXXXXXXXXXXXXXXXXXXXXXXXXXX
00004	(000012)	XXXXXXXXXXXXXX
00005	(000014)	XXXXXXXXXXXXXX
00006	(000005)	XXXXXX
00007	(000006)	XXXXXX
00008	(000002)	IXX
00009	(000005)	XXXXXX
00010	(000000)	I
00011	(000002)	IXX
00012	(000000)	I
00013	(000000)	I
00014	(000000)	I
00015	(000000)	I
00016	(000001)	IX

OVER (000000) I

CALCULATIONS/SUMMARY

NUMBER	0.10000-03
MEAN	0.33880-00
VARIANCE	0.11617-00
STD. DEV.	0.34084-00
SKEWNESS	-0.16974-01
KURTOSIS	0.18730-02

RETRIEVAL DISTRIBUTION

FIG. 10

CELL WIDTH 0.100 X 852 - 1/4 WATT - 100° - 1000 HZS

CELL NO.	0	10	20	30	40	50

-OVER (00000) 1

-0003 (00001) 1X

-0002 (00003) 1XX

-0001 (00048) 1XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0000 (00021) 1XXXXXXXXXXXXXXXXXXXX

0001 (00023) 1XXXXXXXXXXXXXXXXXXXX

0002 (00001) 1X

0003 (00001) 1X

OVER (00000) 1

CALCULATIONS/SUMMARY

NUMBER 0.10000-03

MEAN -0.14439-01

VARIANCE 0.41348-02

STD. DEV. 0.64302-01

SKEWNESS 0.85892-00

KURTOSIS 0.81397-01

RETRIEVAL DISTRIBUTION

FIG. 11

CELL WIDTH 0.100 E

85°C - 1/4 WATT - 100² - 2000 HOURS

CELL NO.	0	10	20	30	40	50	60

-OVER (00000) 1

-0003 (00002) IXX

-0002 (00004) IXXXX

-0001 (00056) IXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0000 (00018) IXXXXXXXXXXXXXXXXXXXX

0001 (00018) IXXXXXXXXXXXXXXXXXXXX

0002 (00001) IX

0003 (00001) IX

OVER (00000) 1

CALCULATIONS/SUMMARY

NUMBER 0.10000-03

MEAN -0.27268-01

VARIANCE 0.52249-02

STD. DEV. 0.72283-01

SKEWNESS 0.16205-00

KURTOSIS 0.83460-01

RETRIEVAL DISTRIBUTION

F.C. 12

CELL WIDTH 0.100 H 882 - 1/4 WATT - 1000th - 1000 HZ.

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00001) IX

-0047 (00001) IX

-0046 (00000) I

-0045 (00000) I

-0044 (00000) I

-0043 (00000) I

-0042 (00000) I

-0041 (00000) I

-0040 (00000) I

-0039 (00000) I

-0038 (00000) I

-0037 (00000) I

-0036 (00000) I

-0035 (00000) I

-0034 (00000) I

-0033 (00000) I

-0032 (00000) I

-0031 (00000) I

-0030 (00000) I

-0029 (00000) I

-0028 (00000) I

-0027 (00000) I

-0026 (00000) I

-0025 (00000) I

-0024 (00000) I

-0023 (00000) I

-0022 (00000) I

-0021 (00000) I

-0020 (00000) I

-0019 (00000) I

-0018 (00000) I

-0017 (00000) I

-0016 (00000) I

-0015 (00000) I

-0014 (00000) I

-0013 (00000) I

-0012 (00000) I

-0011 (00000) I

-0010 (00000) I

-0009 (00000) I

-0008 (00000) I

-0007 (00000) I

-0006 (00000) I

-0005 (00001) IX

-0004 (00001) IX

-0003 (00003) IXXX

-0002 (00009) IXXXXXXXXXXX

-0001 (00040) IXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0000 (00014) IXXXXXXXXXXXXXXXXXXX

0001 (00010) IXXXXXXXXXXXXXXXXXXXXX

0002 (00000) IXXXXXXXX

0003 (00002) IXX

0004 (00000) I

0005 (00000) I

0006 (00001) IX

0007 (00001) IX

CALCULATIONS/SUMMARY

NUMBER 0.10000-83

MEAN -0.10602-00

VARIANCE 0.10044-01

STD. DEV. 0.13433-01

SKEWNESS -0.03594-01

KURTOSIS 0.75459-02

RETRIEVAL DISTRIBUTION

FIG. 13

CELL WIDTH 0.100 S 852 - 1/4 WATT - 100K - 2000 Hrs

CELL NO.	0	10	20	30	40	50
----------	---	----	----	----	----	----

-OVER (00001) IX

-0034 (00001) IX

-0033 (00000) I

-0032 (00000) I

-0031 (00000) I

-0030 (00000) I

-0049 (00000) I

-0048 (00000) I

-0047 (00000) I

-0046 (00000) I

-0045 (00000) I

-0044 (00000) I

-0043 (00000) I

-0042 (00000) I

-0041 (00000) I

-0040 (00000) I

-0039 (00000) I

-0038 (00000) I

-0037 (00000) I

-0036 (00000) I

-0035 (00000) I

-0034 (00000) I

-0033 (00000) I

-0032 (00000) I

-0031 (00000) I

-0030 (00000) I

-0029 (00000) I

-0028 (00000) I

-0027 (00000) I

-0026 (00000) I

-0025 (00000) I

-0024 (00000) I

-0023 (00000) I

-0022 (00000) I

-0021 (00000) I

-0020 (00000) I

-0019 (00000) I

-0018 (00000) I

-0017 (00000) I

-0016 (00000) I

-0015 (00000) I

-0014 (00000) I

-0013 (00000) I

-0012 (00000) I

-0011 (00000) I

-0010 (00000) I

-0009 (00000) I

-0008 (00000) I

-0007 (00000) I

-0006 (00000) I

-0005 (00000) I

-0004 (00002) IXX

-0003 (00000) I

-0002 (00009) IXXXXXXXXXX

-0001 (00017) IXXXXXXXXXXXXXXXXXXXX

0000 (00010) IXXXXXXXXXXXX

0001 (00029) IXXXXXXXXXXXXXXXXXXXXXXXXXXXX

0002 (00016) IXXXXXXXXXXXXXXXXXXXX

0003 (00009) IXXXXXXXXXX

0004 (00002) IXX

0005 (00002) IXX

0006 (00000) I

0007 (00000) I

0008 (00000) I

0009 (00001) IX

0010 (00000) I

0011 (00001) IX

OVER (00000) I

CALCULATIONS/SUMMARY

NUMBER 0.10000-03

MEAN -0.79361-01

VARIANCE 0.13769-01

STD. DEV. 0.11734-01

SKEWNESS -0.74195-01

KURTOSIS 0.60790-02

RETRIEVAL DISTRIBUTION

F. G. 14

CELL WIDTH 0.100 N 85 E. 1/4 WATT-100K²-3000 WATT

CELL NO. 5 10 20 30 40 50

OVER (00000) I

-0056 (00001) IX
-0055 (00000) I
-0054 (00000) I
-0053 (00000) I
-0052 (00000) I
-0051 (00000) I
-0050 (00000) I
-0049 (00000) I
-0048 (00000) I
-0047 (00000) I
-0046 (00000) I

CALCULATIONS/SUMMARY

-0021 (00000) I
-0020 (00000) I
-0019 (00000) I
-0018 (00000) I
-0017 (00000) I
-0016 (00000) I
-0015 (00000) I
-0014 (00000) I
-0013 (00000) I
-0012 (00000) I
-0011 (00000) I
-0010 (00000) I
-0009 (00000) I
-0008 (00000) I
-0007 (00000) I
-0006 (00000) I
-0005 (00001) IX
-0004 (00001) IX
-0003 (00000) I
-0002 (00004) IXXXX

NUMBER 0.10000-03
MEAN 0.97821-01
VARIANCE 0.41141-02
STD. DEV. 0.64141-00
SKEWNESS -0.63103-01
KURTOSIS 0.59167-02

-0031 (00013) IXXXXXXXXXXXXX
0090 (00000) IXXXXXXXXXX
0001 (00023) IXXXXXXXXXXXXXXXXXXXXX
0092 (00025) IXXXXXXXXXXXXXXXXXXXXXXXXX
0003 (00010) IXXXXXXXXXXXX
0004 (00007) IXXXXXXXXXX
0005 (00000) I
0006 (00002) IXX
0007 (00001) IX
0008 (00000) I
0009 (00000) I
0010 (00000) I
0011 (00001) IX
0012 (00000) I
0013 (00001) IX
0014 (00000) I
0015 (00000) I
0016 (00001) IX
0017 (00001) IX

OVER (00000) I

Fig. 15



NO. 2408-10 BATTERY SHEET PAPER
10 X 10 PER INCH

EUGENE BATTERY CO.
MADE IN U. S. A.

86/4

48 Hour Load Life - 85°C W W

10-25-65

Cumulative Percent

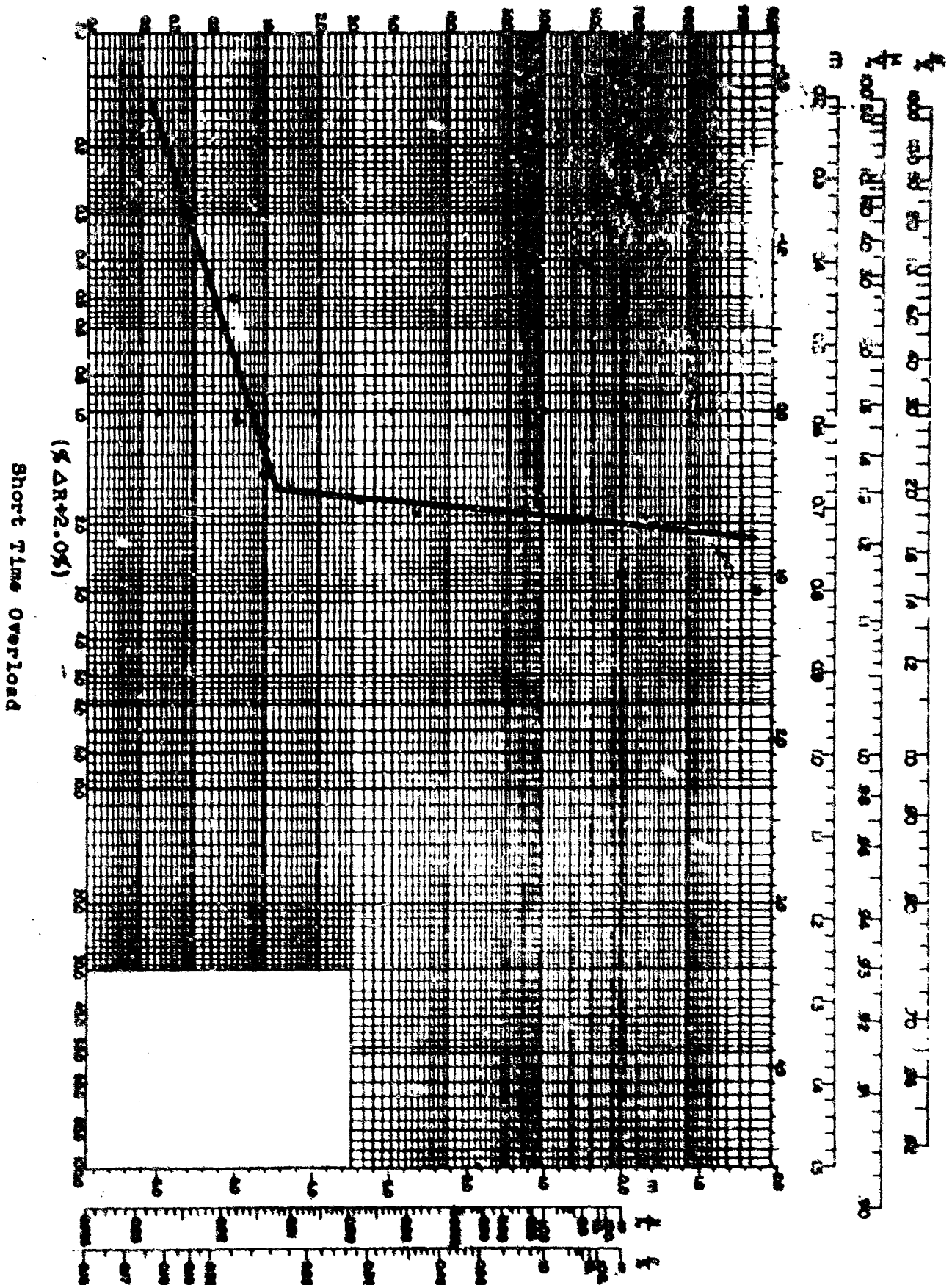


Fig. 19

Cumulative Percent

No Short Time Overload

($\Delta R + 12.0\%$)

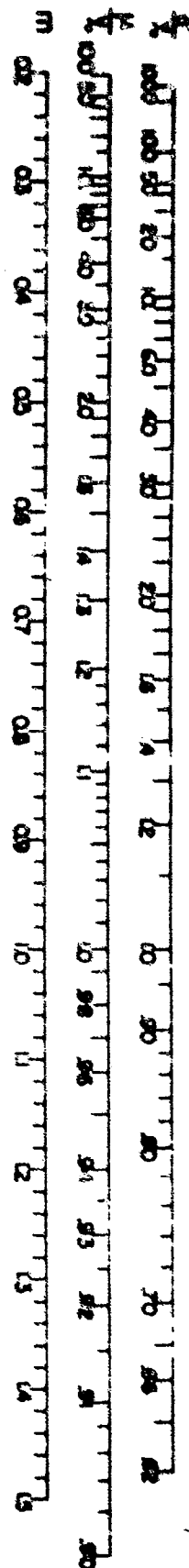
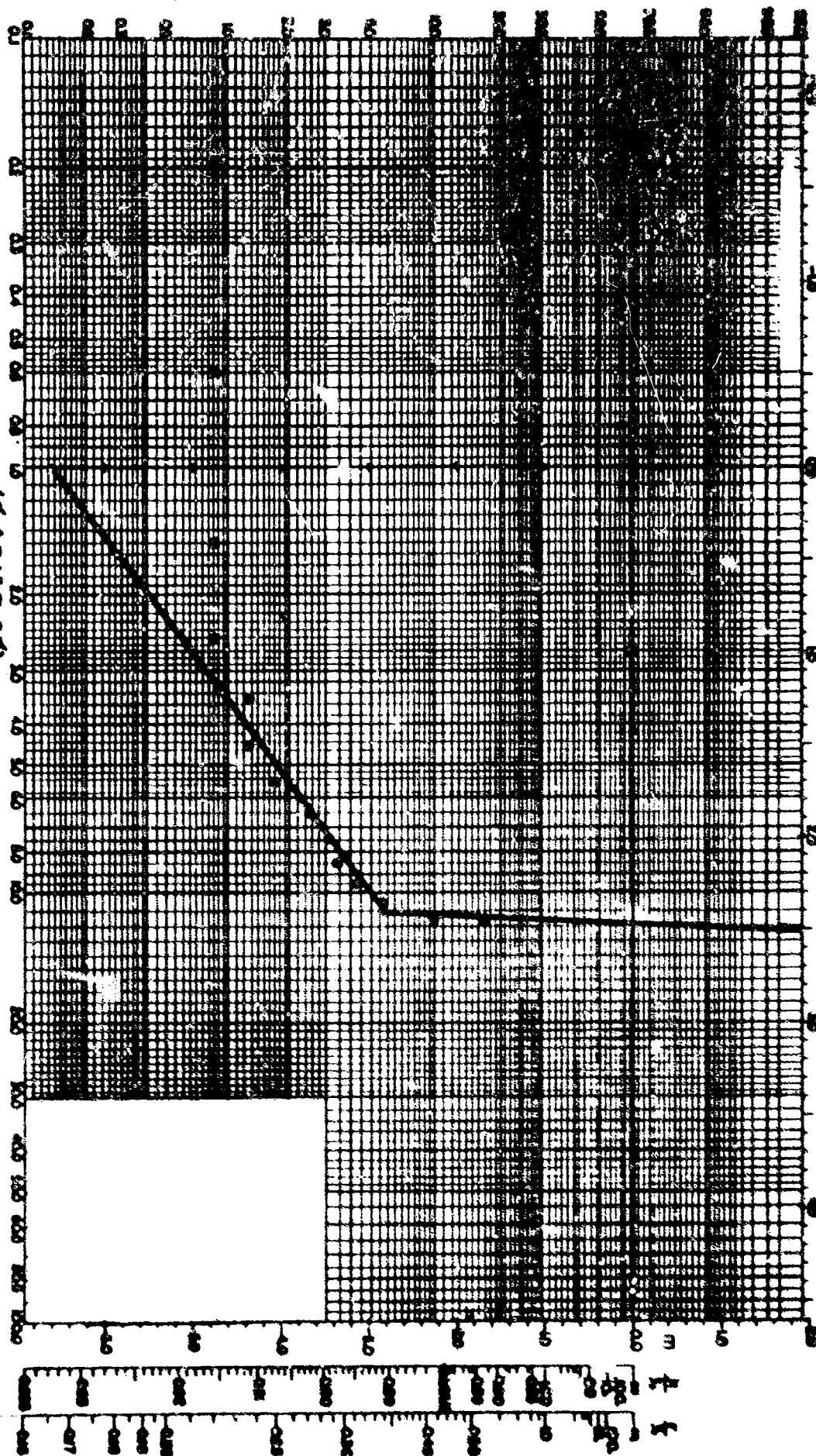


Fig. 19

Fig. 15

°C TEMPERATURE RISE AT 70°C AMBIENT

GOVERNMENT CONTRACT 88-71-20

Resistance	LOAD - WATTS						
	1/8	1/4	3/8	1/2	5/8	3/4	1
10Ω	10.5 9.5	20.8 17.5	26.2 23.5	35.0 36.0	45.4 43.6	47.0 55.5	70.0 75.5
100Ω	11.5 11.0	20.9 21.2	23.4 26.6	37.0 42.0	49.8 51.8	51.0 57.5	62.0 75.7
1KΩ	9.5 9.0	18.5 17.5	26.8 24.8	36.0 33.0	48.0 53.4	49.5 46.0	49.9 63.5
10KΩ	9.5 11.5	20.0 22.5	27.8 31.0	37.0 39.0	52.0 53.4	60.5 60.5	79.3 81.3
39KΩ	10.5 10.5	20.8 21.5	29.5 32.5	35.0 37.0	46.0 49.0	53.0 54.0	73.5 76.5
100KΩ	9.5 7.5	18.2 15.2	28.2 27.5	39.0 36.0	51.8 49.8	56.5 52.0	73.5 68.5
AVG.	10.0	19.5	27.7	36.8	49.9	53.6	70.8
MAX.	11.5	22.5	32.5	42.0	53.4	60.5	81.3
MIN.	7.5	15.2	23.4	33.0	45.4	46.0	49.9

10/8/65

Fig 17

°C TEMPERATURE RISE AT 100°C AMBIENT
GOVERNMENT CONTRACT 88-71-20

	LOAD - WATTS						
	1/8	1/4	3/8	1/2	5/8	3/4	1
10Ω	8.5 11.5	19.0 23.0	21.7 24.5	28.0 34.0	39.6 46.6	48.0 57.0	60.2 67.4
100Ω	13.0 8.5	22.8 24.0	27.3 27.5	31.0 31.0	41.6 41.8	48.2 49.0	59.2 60.8
1KΩ	8.5 12.5	19.5 24.8	25.0 28.9	31.0 34.0	42.8 47.0	50.0 53.0	66.6 70.5
10KΩ	8.5 7.5	15.2 15.8	28.3 26.3	29.0 26.0	40.6 41.4	52.4 52.4	67.2 67.4
39KΩ	11.5 12.5	22.0 25.2	31.0 34.7	36.0 41.0	48.8 52.8	59.0 64.0	76.8 84.8
100KΩ	8.5 8.5	18.6 17.8	29.0 27.0	34.0 32.0	44.8 42.8	53.4 51.4	69.1 65.4
AVG.	9.9	20.7	27.5	32.4	44.2	53.1	67.9
MAX.	13.0	25.2	34.7	41.0	52.8	64.0	84.8
MIN.	7.5	15.2	21.7	28.0	39.6	48.0	59.2

10/8/65

Fig. 20

°C TEMPERATURE RISE AT 125°C AMBIENT

Government Contract SS-71-20

Resistance	LOAD - WATTS						
	1/8	1/4	3/8	1/2	5/8	3/4	1
10Ω	5.0 5.0	12.6 11.6	22.9 21.8	9.0 27.0	48.0 45.4	48.0 46.0	74.0 68.2
100Ω	9.5 9.5	22.5 21.5	25.5 23.5	11.0 32.0	40.6 40.0	47.6 47.0	55.2 51.9
1KΩ	0.0 1.5	11.5 11.5	16.8 21.0	22.0 27.0	34.4 40.4	38.0 43.4	62.4 50.9
10KΩ	3.0 3.5	13.8 12.2	20.8 17.5	28.0 26.0	42.4 38.4	51.0 46.4	72.9 60.4
39KΩ	8.5 9.5	21.0 20.5	29.8 29.2	35.0 36.0	47.4 47.4	54.0 56.0	74.2 74.3
100KΩ	3.5 3.5	14.6 13.8	22.8 22.5	31.0 30.0	41.8 40.0	49.0 45.0	65.8 61.5
AVG.	5.2	15.6	23.0	26.2	42.2	47.6	64.3
MAX.	9.5	22.5	29.8	36.0	48.0	56.0	74.9
MIN.	0.0	11.5	16.8	9.0	34.4	38.0	50.9

10/8/65

Fig. 24

°C TEMPERATURE RISE AT 150°C AMBIENT

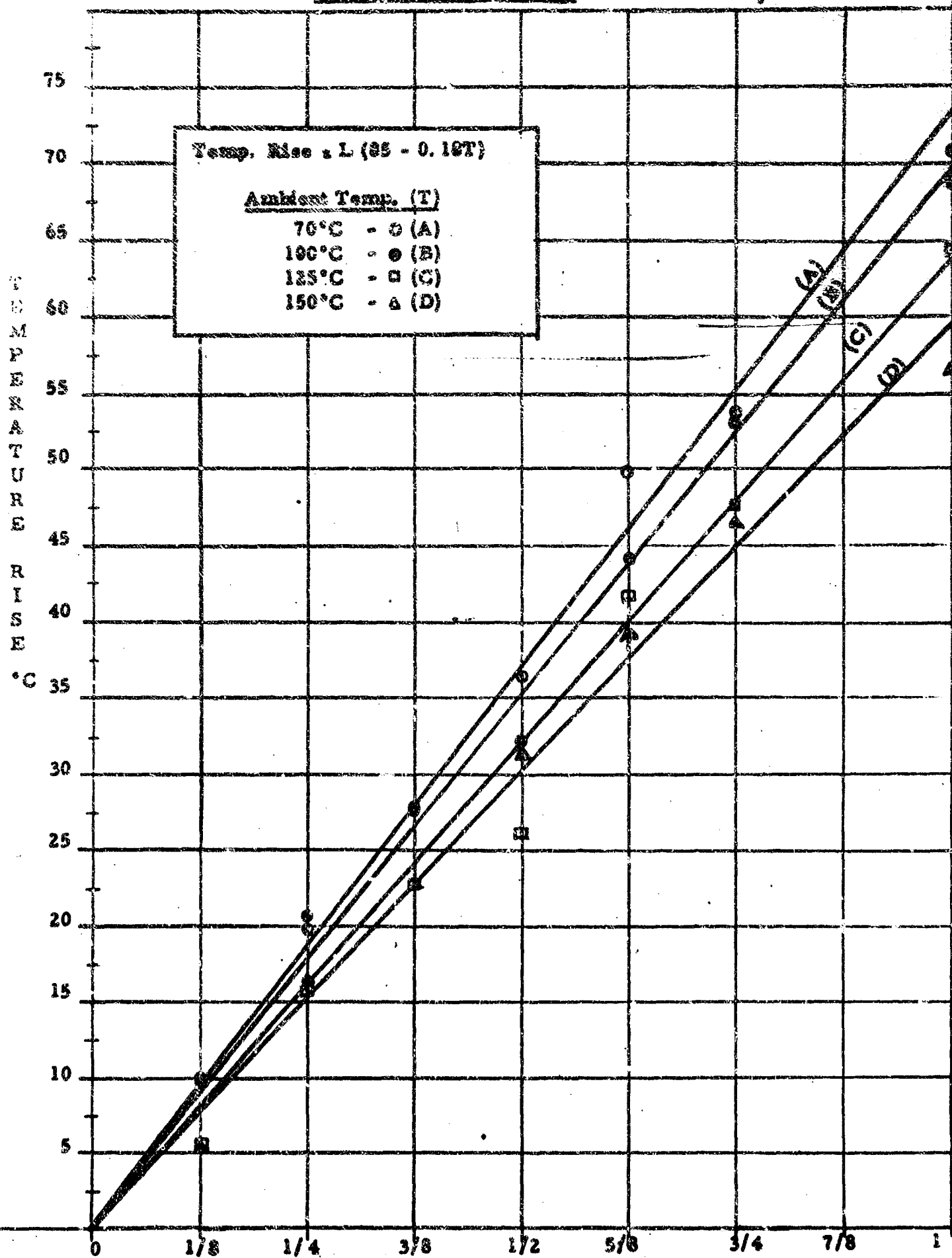
GOVERNMENT CONTRACT 88-71-20

Load	LOAD - WATTS						
	1/8	1/4	3/8	1/2	5/8	3/4	1
10Ω	2.0 3.0	10.0 10.0	20.8 22.6	30.0 29.0	37.4 31.8	42.0 40.0	42.0 42.0
100Ω	9.0 9.5	20.2 22.0	21.8 23.2	27.0 31.0	38.6 40.4	47.4 51.0	63.0 59.0
1KΩ	3.0 4.0	16.2 17.0	22.4 22.4	32.0 32.0	40.7 43.4	45.0 44.5	62.8 61.4
10KΩ	3.0 3.0	14.0 17.0	20.0 24.2	31.0 33.0	34.8 38.4	41.4 47.5	51.6 58.2
39KΩ	9.0 9.0	21.8 22.0	27.4 30.0	35.0 43.0	38.0 45.6	48.0 55.6	54.0 67.5
100KΩ	1.5 4.0	13.0 14.2	19.8 22.2	30.0 33.0	37.8 40.7	51.0 47.0	58.5 59.0
AVG.	5.2	16.4	23.1	32.2	38.9	46.7	56.5
MAX.	9.5	22.0	30.0	43.0	45.6	55.6	67.5
MIN.	1.5	10.0	19.8	27.0	31.8	40.0	42.0

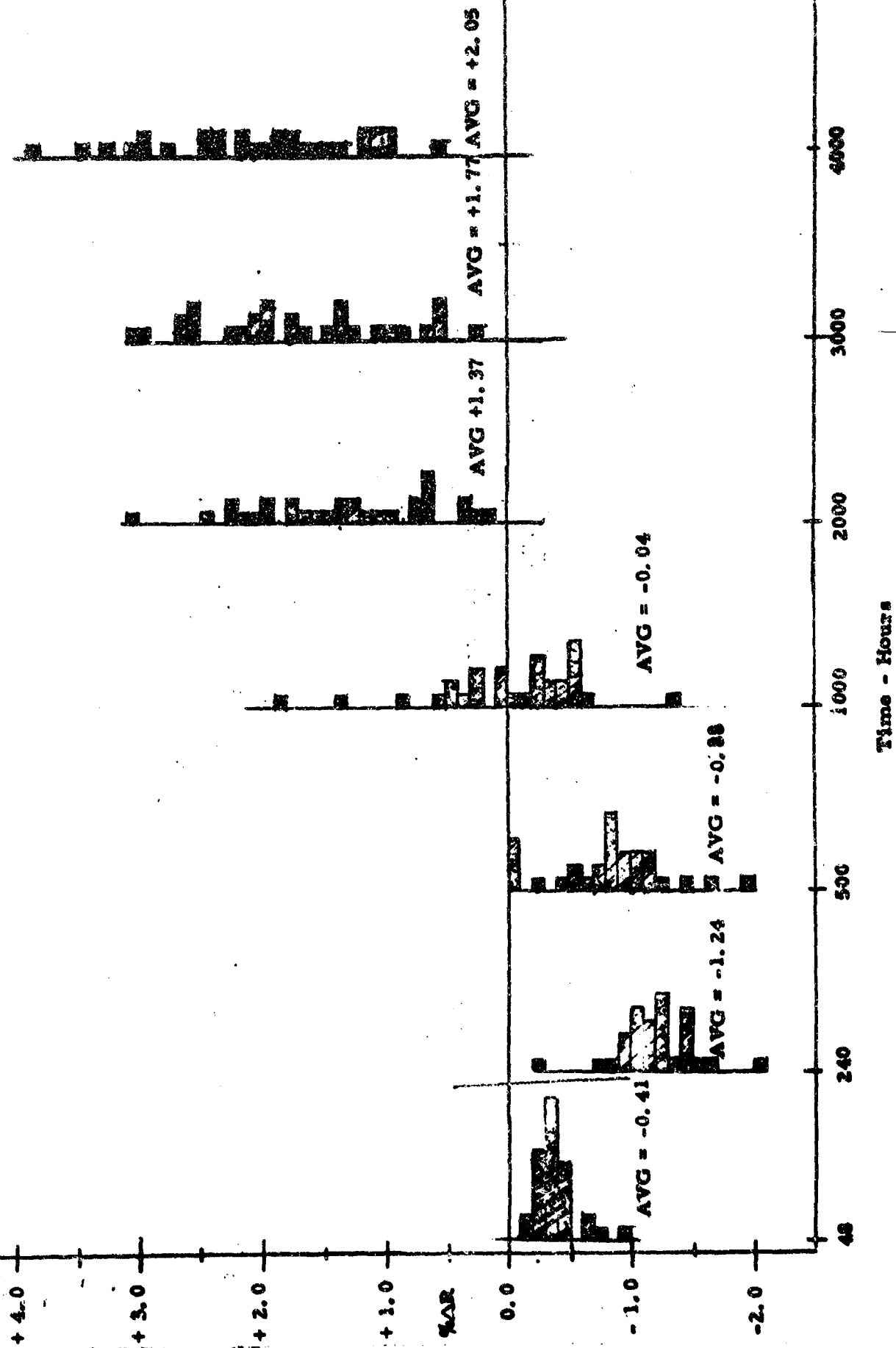
10/8/65

Temperature Rise Curves

Fig. 22



175°C No Load in Air - 10KΩ



175°C No Load in Argon followed by Air - 10KC

Legend:  Argon
 Air

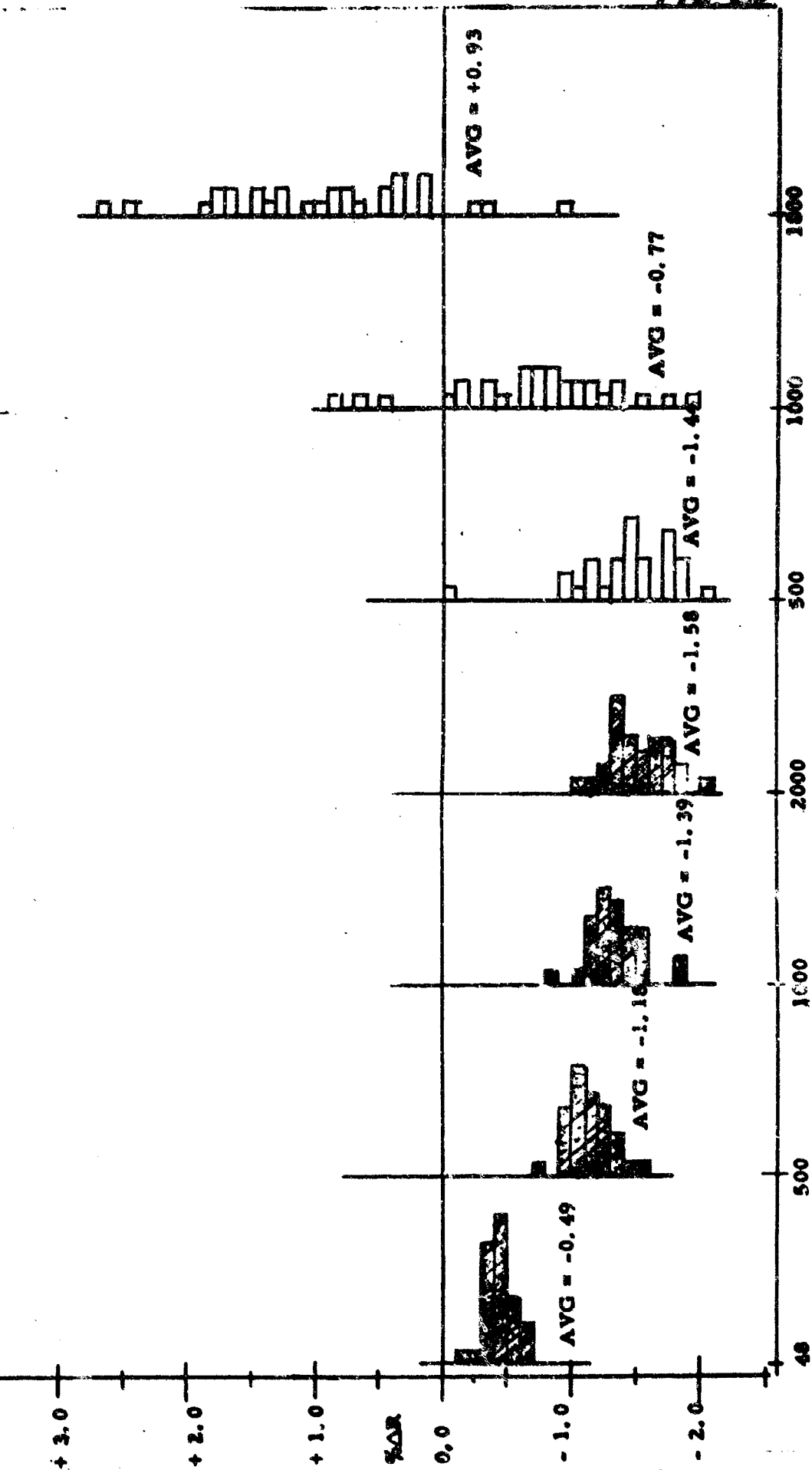


Fig. 24

PREPARED BY: M. DIXON		TITLE SUMMARY OF ML-R-11E PERFORMANCE										CONTRACT PROJECT - 88-71-20		ADD NUMBER - 6					
DESIGNED BY: W. HAWK																			
DRAWN BY: S. MATTIE																			
DESIGNABLE PERCENT CHANGE														3.5%					
RESISTANCE & DATA NO		RESISTANCE - TEMPERATURE CHARACTERISTIC				VOLTAGE COEFFICIENT % PER VOLT		DIELECTRIC STRENGTH		INSULATION STRENGTH (MILES)		DATA NO		TEMPERATURE CYCLE		MOISTURE RESISTANCE			
		75	35	46.5	70.5														
10Ω 30252	AVERAGE	2.64	0.83	2.87	4.37	NA		—		ALL		3		20.10	20.1	20.50	20.7	20.50	20.7
	SPAN	0.20	0.40	4.73	8.92			—		10.5		2		17.51	17.20	17.21	10.4	17.0	10.4
	FAIL	0.90	7.22	2.50	7.10			—		ALL		3		20.10	20.9	20.09	20.0	20.10	20.0
10Ω 30258	AVERAGE	2.71	1.10	4.08	4.63	NA		—		ALL		3		20.09	20.06	20.56	20.7	20.66	20.7
	SPAN	2.61	2.61	4.68	2.22			—		10.5		2		17.51	17.20	17.21	10.4	17.0	10.4
	FAIL	0.91	7.41	20.60	7.30			—		ALL		3		20.09	20.0	20.0	20.0	20.0	20.0
10Ω 30264	AVERAGE	2.64	1.01	4.93	4.64	NA		—		ALL		3		20.05	20.07	20.42	20.7	20.36	20.7
	SPAN	2.60	2.60	4.32	2.21			—		10.5		2		17.51	17.20	17.21	10.4	17.0	10.4
	FAIL	0.80	7.87	20.50	8.02			—		ALL		3		20.05	20.0	20.0	20.0	20.0	20.0
100Ω 30270	AVERAGE	2.73	2.20	2.13	2.52	NA		—		ALL		3		20.02	20.09	20.43	20.7	20.72	20.7
	SPAN	2.70	5.75	2.02	7.02			—		10.5		2		17.51	17.20	17.21	10.4	17.0	10.4
	FAIL	2.30	2.84	2.74	2.09			—		ALL		3		20.07	20.09	20.28	20.7	20.20	20.7
100Ω 30276	AVERAGE	2.60	2.15	2.32	2.66	NA		—		ALL		3		20.04	20.03	20.55	20.7	20.40	20.7
	SPAN	2.78	5.76	2.16	7.21			—		10.5		2		17.51	17.20	17.21	10.4	17.0	10.4
	FAIL	2.10	2.85	2.13	2.50			—		ALL		3		20.01	20.10	20.37	20.7	20.17	20.7
100Ω 30282	AVERAGE	2.21	5.91	2.33	2.85	NA		—		ALL		3		20.01	20.03	20.42	20.7	20.29	20.7
	SPAN	2.87	5.47	2.04	7.07			—		10.5		2		17.51	17.20	17.21	10.4	17.0	10.4
	FAIL	2.65	6.17	2.14	20.50			—		ALL		3		20.0	20.07	20.27	20.7	20.17	20.7
1K 30288	AVERAGE	0.92	2.57	4.00	2.13	+0.0166		—		ALL		3		20.05	20.06	20.35	20.7	20.31	20.7
	SPAN	0.96	0.70	4.42	2.84	+0.0034		—		10.5		2		17.24	17.03	17.52	10.4	17.52	10.4
	FAIL	7.62	2.88	20.66	4.85	+0.0014		—		ALL		3		20.05	20.07	20.19	20.7	20.06	20.7
1K 30294	AVERAGE	0.77	4.31	2.87	2.87	+0.00154		—		ALL		3		20.03	20.04	20.42	20.7	20.26	20.7
	SPAN	0.13	2.01	4.76	2.87	+0.0027		—		10.5		2		17.07	17.20	17.18	10.4	17.09	10.4
	FAIL	7.88	2.23	20.13	20.77	+0.000		—		ALL		3		20.09	20.03	20.13	20.7	20.09	20.7
1K 30300	AVERAGE	0.87	7.61	4.02	2.34	+0.00193		—		ALL		3		20.04	20.05	20.40	20.7	20.53	20.7
	SPAN	2.58	7.08	4.20	2.62	+0.0034		—		10.5		2		17.10	17.03	17.45	10.4	17.18	10.4
	FAIL	7.31	20.50	4.71	4.57	+0.0014		—		ALL		3		20.0	20.0	20.35	20.7	20.27	20.7
10K 30306	AVERAGE	2.64	20.47	20.47	20.15	+0.00148		—		ALL		3		20.01	20.05	20.21	20.7	20.54	20.7
	SPAN	10.28	4.21	20.09	10.19	+0.0002		—		10.5		2		17.03	17.00	17.35	10.4	17.04	10.4
	FAIL	0.0	20.02	20.11	20.72	+0.0025		—		ALL		3		20.04	20.10	20.11	20.7	20.29	20.7
10K 30312	AVERAGE	2.25	20.54	20.11	20.41	+0.00193		—		ALL		3		20.10	20.05	20.30	20.7	20.33	20.7
	SPAN	20.30	4.05	20.12	20.20	+0.0007		—		10.5		2		17.10	17.10	17.58	10.4	17.55	10.4
	FAIL	0.10	20.18	20.23	20.28	+0.0035		—		ALL		3		20.02	20.0	20.33	20.7	20.09	20.7
10K 30318	AVERAGE	2.26	20.62	20.06	20.49	+0.00225		—		ALL		3		20.04	20.06	20.41	20.7	20.47	20.7
	SPAN	20.60	20.85	20.18	20.07	+0.0011		—		10.5		2		17.09	17.10	17.20	10.4	17.14	10.4
	FAIL	20.04	20.17	20.23	20.33	+0.0050		—		ALL		3		20.12	20.0	20.39	20.7	20.21	20.7

NOTE: MATHEMATIC. AVERAGES OF ABSOLUTE CHANGES ARE SHOWN WITH ± INDICATOR

CHARACTERISTICS

AND BINDER - 66-6

TYPE

P6

B-FIGURE 23

DATE - FEB 10, 1965

MOISTURE RESISTANCE					DATA N2	70° LOAD LIFE HOURS					DATA N2	TERMINAL STRENGTH	EFFECT OF SOLDERING	DATA N2	SMOK TEST	H - FREQUENCY VIBRATION	DATA N2	SOLDER- ABILITY
LOAD	INSULATION RESISTANCE (MEG.)	NO LOAD	INSULATION RESISTANCE (MEG.)	SHORT TIME OVER LOAD		98	2-2	50	750	1000								
0.50	10.7	10.58	10.7	10.08	3	0.0	0.0	0.0	0.0	10.12	3	10.05	10.06	3	10.10	10.06	3	1
1.0	10.4	11.0	10.4	10.51	0	0.0	0.0	0.0	0.0	10.50	0	10.10	10.20	2	10.30	10.50	2	1
2.0	10.0	11.0	10.0	10.10	2	0.0	0.0	0.0	0.0	10.10	2	10.20	10.0	5	10.10	10.0	5	1
5.0	9.5	9.5	9.5	0	4	0	0	0	0	0	5	0	0	6	0	0	7	0
10.0	10.7	10.66	10.7	10.11	3	10.01	10.02	10.14	10.08	10.07	3	10.01	10.08	3	10.02	10.06	3	1
20.0	10.4	11.0	10.4	11.00	0	10.0	10.10	10.80	10.20	10.10	0	10.0	10.10	2	10.10	10.30	2	1
50.0	10.0	10.0	10.0	0.0	6	10.10	10.10	10.10	10.40	10.10	6	10.10	10.40	6	10.0	10.0	6	1
100.0	0.5	9.5	9.5	0	0	0	0	0	0	0	1	0	0	2	0	0	3	0
200.0	10.7	10.36	10.7	10.16	3	0.0	0.0	10.03	10.05	10.04	3	10.02	10.04	3	10.03	10.05	3	1
500.0	10.0	10.80	10.0	10.50	0	0.0	0.0	0.0	10.10	10.10	0	10.10	10.30	3	10.10	10.20	3	1
1000.0	2.5	10.0	10.0	0.0	2	0.0	0.0	10.10	10.10	10.10	2	10.10	0.0	6	0.0	10.10	6	1
2000.0	9.5	9.5	9.5	0	6	0	0	0	0	0	7	0	0.19	8	0	0	9	0
5000.0	10.7	10.72	10.7	10.05	3	10.10	10.05	10.73	10.03	10.07	3	10.05	10.11	3	10.02	10.11	3	1
10000.0	10.4	11.26	10.4	10.0	0	10.10	10.64	10.14	10.37	10.25	0	10.0	10.20	2	10.0	10.20	2	1
20000.0	10.0	10.0	10.0	0.10	2	10.06	0.0	10.08	0.0	10.04	2	10.10	10.03	7	10.0	10.10	7	1
50000.0	9.5	9.5	9.5	0	12	0	0	0	0	0	13	0	0	14	0	0	15	0
100000.0	10.55	10.50	10.55	10.05	3	10.07	10.53	10.62	10.97	10.26	3	10.01	10.09	3	10.04	10.16	3	1
200000.0	10.0	10.57	10.0	10.0	2	10.29	10.29	10.74	10.54	10.97	2	10.01	10.12	3	10.0	10.21	3	1
500000.0	10.37	10.17	10.37	10.09	7	10.02	10.18	10.17	10.32	10.46	7	10.10	10.03	8	10.10	10.10	8	1
1000000.0	9.5	9.5	9.5	0	8	0	0	0	0	0	1	0	0	8	0	0	1	0
2000000.0	10.7	10.29	10.7	10.04	3	10.08	10.50	10.66	10.02	10.39	3	10.06	10.10	3	10.03	10.10	3	1
5000000.0	10.54	10.53	10.54	10.10	0	10.27	10.22	10.69	10.10	10.34	0	10.0	10.00	2	10.04	10.14	2	1
10000000.0	10.27	10.17	10.27	10.05	8	10.02	10.16	10.16	10.27	10.35	8	10.10	0.0	8	10.0	10.0	8	1
20000000.0	9.5	9.5	9.5	0	4	0	0	0	0	0	5	0	0	6	0	0	7	0
50000000.0	10.34	10.31	10.34	10.03	3	10.06	10.11	10.11	10.14	10.15	3	10.09	10.02	3	10.03	10.16	3	1
100000000.0	10.52	10.52	10.52	0.0	0	10.10	10.20	10.20	10.22	10.34	0	10.04	10.06	2	10.04	10.08	2	1
200000000.0	10.19	10.06	10.19	10.18	9	0.0	10.02	0.0	10.02	10.03	9	0.11	10.07	9	10.0	10.0	9	1
500000000.0	9.5	9.5	9.5	0	0	0	0	0	0	0	1	0	0	2	0	0	3	0
1000000000.0	10.42	10.26	10.42	10.05	3	10.02	10.10	10.10	10.12	10.15	3	10.02	10.01	3	10.02	10.12	3	1
2000000000.0	10.14	10.39	10.14	10.10	0	10.07	10.27	10.27	10.39	10.39	0	10.03	10.05	2	10.07	10.17	2	1
5000000000.0	10.13	10.09	10.13	10.12	2	0.0	10.04	10.03	10.03	10.10	9	10.05	10.01	9	10.0	10.07	9	1
10000000000.0	9.5	9.5	9.5	0	16	0	0	0	0	0	7	0	0	8	0	0	9	0
20000000000.0	10.14	10.53	10.14	10.03	3	10.07	10.14	10.14	10.17	10.20	3	10.05	10.01	3	10.05	10.13	3	1
50000000000.0	10.44	10.18	10.44	10.10	3	10.30	10.29	10.29	10.29	10.44	3	10.07	10.03	3	10.06	10.20	3	1
100000000000.0	10.25	10.27	10.25	10.11	0	10.01	10.06	10.06	10.08	10.08	0	10.00	10.0	4	10.01	10.05	4	1
200000000000.0	9.5	9.5	9.5	0	2	0	0	0	0	0	3	0	0	4	0	0	5	0
500000000000.0	10.21	10.54	10.21	10.04	3	10.03	10.4	10.4	10.15	10.17	3	10.02	10.10	3	10.01	10.05	3	1
1000000000000.0	10.35	10.51	10.35	10.16	0	10.08	10.18	10.20	10.21	10.24	0	10.04	10.16	3	10.05	10.07	3	1
2000000000000.0	10.11	10.29	10.11	10.11	3	10.01	10.02	10.04	10.04	10.05	3	10.03	10.01	3	10.0	10.04	3	1
5000000000000.0	9.5	9.5	9.5	0	8	0	0	0	0	0	9	0	0	10	0	0	11	0
10000000000000.0	10.36	10.33	10.36	10.10	3	10.19	10.15	10.17	10.20	10.21	3	10.17	10.15	3	10.01	10.06	3	1
20000000000000.0	10.55	10.50	10.55	10.10	3	10.01	10.25	10.23	10.23	10.25	3	10.05	10.10	3	10.03	10.10	3	1
50000000000000.0	10.22	10.09	10.22	10.50	14	10.14	10.23	10.29	10.23	10.14	1	10.01	10.22	1	10.03	10.04	1	1
100000000000000.0	9.5	9.5	9.5	0	0	0	0	0	0	0	5	0	0	6	0	0	17	0
200000000000000.0	10.11	10.47	10.11	10.15	3	10.21	10.14	10.14	10.18	10.22	3	10.10	10.24	3	10.01	10.04	3	1
500000000000000.0	10.20	10.14	10.20	10.07	3	10.10	10.20	10.25	10.25	10.26	3	10.21	10.19	3	10.05	10.08	3	1
1000000000000000.0	10.34	10.08	10.34	10.23	2	10.24	10.08	10.05	10.05	10.10	2	0.0	10.30	2	0.0	0.0	2	1
2000000000000000.0	9.5	9.5	9.5	0	0	0	0	0	0	0	1	0	10.00	2	0	5	3	0

WITH 100% INDICATING THE MAJORITY CLASS OF ELECTRICAL CHANGES.

2

DESIGNED BY: M. D. KORN		TITLE: SUMMARY OF H-R-11E PERFORMANCE CHARACTERISTICS													
DESIGNED BY: W. H. WALK		CONTRACT PROJECT 88.710													
DESIGNED BY: S. MATTIE		HOLD POW-DE													
ALLOWABLE PERCENT CHANGE		2.5%													
RESISTANCE & DATA NO		RESISTANCE - TEMPERATURE CHARACTERISTIC				VOLTAGE COEFFICIENT % PER VOLT	DIELECTRIC STRENGTH	INSULATION STRENGTH (MINS)	DATA NO	LOW TEMP OPERATION	TEMPERATURE CYCLE	MOISTURE RESISTANCE			
		18% 1.4% 3.2% 3.4%										LOAD	COLLATION (MINS.)	NO LOAD	TEST
		75	85	145	165										
39K 30324	AVERAGE	50.4	49.30	44.10	44.25	-0.0357	—	ALL	30	2.02	2.02	1.15	ALL	2.27	ALL
	SPAN	11.10	10.25	10.36	10.47	-0.009	—	10 ⁵	30	1.02	1.15	1.05	10 ⁵	1.05	10 ⁵
	FAIL	0	0	0	0	0	0	0	35	0	0	0	0	0	0
39K 30330	AVERAGE	50.10	50.20	50.19	50.25	-0.0207	—	ALL	30	2.08	2.08	2.22	ALL	2.25	ALL
	SPAN	11.35	10.40	10.08	10.17	-0.015	—	10 ⁵	30	1.50	1.22	1.05	10 ⁵	1.05	10 ⁵
	FAIL	0	0	0	0	0	0	0	35	0	0	0	0	0	0
39K 30336	AVERAGE	50.09	50.25	50.10	50.20	-0.0398	—	ALL	30	2.04	2.04	2.17	ALL	2.44	ALL
	SPAN	11.10	10.08	10.08	10.18	-0.015	—	10 ⁵	30	1.03	1.27	1.07	10 ⁵	1.07	10 ⁵
	FAIL	0	0	0	0	0	0	0	35	0	0	0	0	0	0
62K 30342	AVERAGE	4.36	4.98	7.21	7.22	-0.0380	—	ALL	30	2.02	2.02	2.01	ALL	2.07	ALL
	SPAN	2.63	4.51	7.20	7.67	-0.0074	—	10 ⁵	30	1.05	1.05	1.05	10 ⁵	1.05	10 ⁵
	FAIL	1	2	1	1	3	0	0	35	0	0	0	0	0	0
62K 30348	AVERAGE	4.97	4.04	7.94	7.79	-0.0395	—	ALL	30	2.04	2.04	2.04	ALL	2.04	ALL
	SPAN	4.18	4.47	7.87	7.65	-0.0077	—	10 ⁵	30	1.06	1.06	1.06	10 ⁵	1.06	10 ⁵
	FAIL	4	4	1	1	3	0	0	35	2.02	2.02	2.02	10 ⁵	2.02	10 ⁵
62K 30354	AVERAGE	4.28	4.81	7.67	7.24	-0.05239	—	ALL	30	2.02	2.02	2.02	ALL	2.02	ALL
	SPAN	4.04	4.26	7.26	7.82	-0.0079	—	10 ⁵	30	1.02	1.02	1.02	10 ⁵	1.02	10 ⁵
	FAIL	5	—	4	4	3	0	0	35	1	0	0	0	0	0
100K 03631	AVERAGE	0.82	1.58	0.54	0.98	-0.00771	—	ALL	0	0.01	0.01	0.20	ALL	0.34	ALL
	SPAN	0.22	0.46	0.28	0.45	-0.0049	—	10 ⁵	30	0.0	0.07	0.57	10 ⁴	0.57	10 ⁴
	FAIL	0	0	0	0	-0.0109	—	MEGS	32	0.06	0.0	0.16	MEGS	0.16	MEGS
100Ω 04573	AVERAGE	7.27	2.43	1.12	2.10	—	—	—	045	0.02	0.02	0.04	ALL	0.06	ALL
	SPAN	1.20	2.22	1.12	2.24	NA	—	—	045	0.02	0.02	0.20	10 ⁴	0.2	10 ⁵
	FAIL	0	0	0	0	—	0	0	4	0	0	0	0	0	0
100Ω 04579	AVERAGE	1.35	2.45	1.76	2.18	—	—	—	045	0.04	0.02	0.03	ALL	0.05	ALL
	SPAN	1.20	2.37	1.35	2.26	NA	—	—	045	0.10	0.03	0.09	10 ⁴	0.12	10 ⁵
	FAIL	0	0	0	0	—	0	0	80	0.0	0.05	0.0	MEGS	0.01	MEGS
100Ω 04585	AVERAGE	1.24	2.35	1.13	2.15	—	—	—	045	0.05	0.05	0.03	ALL	0.05	ALL
	SPAN	0.74	1.84	1.22	2.22	NA	—	—	045	0.10	0.0	0.09	10 ⁵	0.20	10 ⁵
	FAIL	0	0	0	0	—	0	0	6	0	0	0.03	MEGS	0.0	MEGS
1	AVERAGE														
	SPAN														
	FAIL														

NOTE: ARITHMETIC AVERAGES OF ABSOLUTE CHANGES ARE SHOWN WITH ± OR + INDICATING

DATE - FEB. 10, 1965

16

\pm OR \mp INDICATING THE MAJORITY CLASS OF BIDIRECTIONAL CHANGES.

PREPARED BY
CHECKED BY
APPROVED BY

TITLE MOISTURE LOAD MATRIX - NO LOAD, 1/20 WATT
CONTRACT PROJECT 68-740

100.0

RESISTANCE
&
DATA NO.

98-100% RH @ 55°C

		48	100	250	500	750	1000	2000												
30942	AV	±0.45	±0.95	±0.11	±0.45	±0.12	±0.17	±0.22												
10Ω	AV	±0.20	±0.20	±0.10	±0.20	±0.10	±0.10	±0.20												
	AV	±0.10	±0.20	±0.10	±0.10	±0.10	±0.10	±0.10												
10Ω	AV	0	0	0	0	0	0	0												
30943	AV	±0.25	±0.30	±0.15	±0.15	±0.15	±0.15	±0.30												
10Ω	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
10Ω	AV	0	0	0	0	0	0	0												
30944	AV	±0.50	±0.50	±0.25	±0.25	±0.25	±0.25	±0.25												
10Ω	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
10Ω	AV	0	0	0	0	0	0	0												
30945	AV	±0.12	±0.27	±0.24	±0.24	±0.24	±0.24	±0.24												
100Ω	AV	±0.20	±0.27	±0.27	±0.27	±0.27	±0.27	±0.27												
	AV	±0.20	±0.27	±0.27	±0.27	±0.27	±0.27	±0.27												
100Ω	AV	0	0	0	0	0	0	0												
30946	AV	±0.18	±0.35	±0.60	±0.35	±0.37	±0.37	±0.37												
100Ω	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	0	0	0	0	0	0	0												
30947	AV	±0.25	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	0	0	0	0	0	0	0												
30948	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
10Ω	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
10Ω	AV	0	0	0	0	0	0	0												
30949	AV	±0.20	±0.20	±0.20	±0.20	±0.20	±0.20	±0.20												
10Ω	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
10Ω	AV	0	0	0	0	0	0	0												
30950	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
10Ω	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
	AV	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10	±0.10												
10Ω	AV	0	0	0	0	0	0	0												
30951	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	0	0	0	0	0	0	0												
30952	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	0	0	0	0	0	0	0												
30953	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
	AV	±0.20	±0.37	±0.37	±0.37	±0.37	±0.37	±0.37												
100Ω	AV	0	0	0	0	0	0	0												

*. 98 LEAD TIME AT END OF TEST * GRIPS CONCEALED

6 LOAD, $\frac{1}{2}$ WATT - 10m, 100m,

TYPE

DWG. NO. 3

FIGURE 27

PO

DATE

WAVE NUMBER - 1000

98/10/16 RH @ 500 Feet

48 100 200 300 400 500 600

100.0	±0.07	±1.03	±1.05	±1.06	±0.20	±0.37	±0.66
04688	±1.17	±2.34	±2.35	±1.52	±0.67	±1.07	±1.67
	-0.30	-2.25	-2.25	-0.27	-0.30	-1.10	-0.60
100.0	0	0	0	0	0	0	0
100.0	±0.06	±1.05	±1.05	±1.06	±0.37	±0.63	±0.66
	+0.30	+3.09	+2.59	+1.52	+0.69	+1.07	+2.10
04689	-0.05	-2.57	-2.59	-0.01	-1.10	-1.10	-0.30
100.0	0	0	0	0	0	0	0
100.0	±0.01	±1.03	±1.09	±1.17	±1.24	±0.44	±2.15
	+0.31	+2.20	+2.30	+0.65	+1.60	+1.10	+1.22
04690	-0.06	-1.80	-1.82	-1.11	-0.20	-1.32	-1.57
100.0	0	0	0	0	0	0	0

100.0	±0.07	±0.56	±0.50	±0.56	±0.56	±0.09	±0.12
04691	±0.15	±1.48	±1.57	±1.57	±1.17	±1.64	±1.39
	-0.30	-1.89	-1.88	-1.10	-2.03	-1.07	-0.60
100.0	0	0	0	0	0	0	0
100.0	±0.03	±0.85	±0.85	±0.85	±0.85	±0.07	±0.10
04692	±0.15	±2.20	±2.20	±1.00	±0.60	±0.20	±0.30
	-0.07	-1.71	-1.71	-2.09	-1.15	-2.45	-0.60
100.0	0	0	0	0	0	0	0
100.0	±0.008	±0.90	±0.91	±0.85	±0.85	±0.07	±0.17
04693	±0.04	±2.12	±2.12	±1.00	±0.60	±0.20	±0.30
	-0.01	-2.05	-1.88	-1.08	-2.05	-0.00	-0.00
100.0	0	0	0	0	0	0	0

GROUPS CANCELLED TO BE REPEATED

PREPARED BY
CHECKED BY
APPROVED BY

TITLE	MOISTURE	LOAD	MATRIX	NO LOAD	$\frac{1}{10}$ LOAD
-------	----------	------	--------	---------	---------------------

CONTRACT PROJECT - 88-71-20

98-100% RH @ 55°C

RESISTANCE		98-100% RH @ 55°C							
DATA NO.		48	100	200	500	1000	2000		
30954	AV	10.12	10.23	10.16	10.15	10.23	10.19	10.22	
1K	AV	10.20	10.23	10.21	10.21	10.16	10.17	10.22	
10K	AV	10.0	10.03	10.16	10.20	10.21	10.22	10.22	
100K	AV	0	0	0	0	0	0	0	
30955	AV	10.11	10.23	10.24	10.21	10.21	10.21	10.21	
1K	AV	10.11	10.23	10.26	10.27	10.22	10.22	10.23	
10K	AV	10.12	10.13	10.27	10.28	10.47	10.47	10.23	
100K	AV	0	0	0	0	0	0	0	
30956	AV	10.07	10.16	10.22	10.27	10.26	10.22	10.27	
1K	AV	10.14	10.26	10.29	10.25	10.28	10.28	10.28	
10K	AV	10.07	10.06	0.0	0.0	10.10	10.10	10.10	
100K	AV	0	0	0	0	0	0	0	
30957	AV	10.24	10.38	10.34	10.73	10.82	10.48	10.28	
1K	AV	10.27	10.64	10.40	10.22	10.50	10.22	10.24	
10K	AV	10.27	10.17	10.17	10.17	10.27	10.25	10.68	
100K	AV	0	0	0	0	0	0	0	
30958	AV	10.27	10.36	10.43	10.28	10.83	10.34	10.18	
1K	AV	10.32	10.27	10.27	10.26	10.06	10.23	10.47	
10K	AV	10.10	10.12	10.03	10.03	10.03	10.30	10.80	
100K	AV	0	0	0	0	0	0	0	
30959	AV	10.36	10.45	10.53	10.59	10.4	10.44	10.20	
1K	AV	10.37	10.42	10.41	10.40	10.4	10.44	10.40	
10K	AV	10.13	10.18	10.24	10.17	10.27	10.15	10.26	
100K	AV	0	0	0	0	0	0	0	
30960	AV	10.24	10.11	10.31	10.53	10.00	10.44	10.22	
1K	AV	10.50	10.23	10.11	10.12	10.37	10.32	10.12	
10K	AV	0.0	0.0	10.34	10.29	10.28	10.22	10.25	
100K	AV	0	0	0	0	0	0	0	
30961	AV	10.06	10.10	10.10	10.15	10.18	10.22	10.12	
1K	AV	10.18	10.17	10.17	10.19	10.22	10.23	10.18	
10K	AV	10.05	0.0	10.01	0.0	10.06	10.02	10.11	
100K	AV	0	0	0	0	0	0	0	
30962	AV	10.07	10.10	10.13	10.14	10.29	10.40	10.58	
1K	AV	10.17	10.20	10.27	10.22	10.23	10.23	10.06	
10K	AV	0.0	10.02	10.06	10.07	10.09	10.11	10.11	
100K	AV	0	0	0	0	0	0	0	
30963	AV	10.19	10.25	10.44	10.53	10.70	10.37	10.74	
1K	AV	10.24	10.38	10.12	10.26	10.45	10.36	10.20	
10K	AV	10.07	10.14	10.21	10.24	10.31	10.55	10.10	
100K	AV	0	0	0	0	0	0	0	
30964	AV	10.67	10.19	10.37	10.38	10.57	10.84	10.21	
1K	AV	10.26	10.31	10.41	10.26	10.30	10.55	10.23	
10K	AV	10.07	10.10	10.17	10.27	10.17	10.24	10.43	
100K	AV	0	0	0	0	0	0	0	
30965	AV	10.20	10.23	10.22	10.37	10.45	10.67	10.03	
1K	AV	10.26	10.27	10.37	10.21	10.23	10.55	10.06	
10K	AV	10.10	10.08	10.14	10.07	10.21	10.24	10.42	
100K	AV	0	0	0	0	0	0	0	

* UNIT # 3- BODY CRACKED

WAD to UNIT - 1X, 10X

WAD FINDER - PREP

R.

DATE

2

BODY CRACKED WHILE BEING REMOVED FROM BACK

PREPARED BY

CHECKED BY

APPROVED BY

TITLE MOISTURE LOAD MATRIX

NO LOAD / NO W -

RESISTANCE

DATA NO.

98-100 TO RH @ 55C

45 100 200 300 400 500 600 700

30966
394

AV
FAIL

10.17 11.13 11.30 11.85 12.41 11.87 11.90
10.10 10.82 11.44 11.97 11.84 11.10 11.42
10.08 10.12 11.12 10.41 11.86 10.28 10.27

30967
394

AV
FAIL

10.21 10.18 11.37 11.89 11.60 11.84 11.06
10.35 11.46 11.65 11.86 11.52 11.20 11.78
10.05 10.10 11.12 11.08 11.36 10.25 10.28

30968
394

AV
FAIL

10.17 10.87 10.34 11.41 11.39 11.64 11.98
10.35 10.49 11.62 11.77 11.77 11.96 11.28
10.07 10.10 10.20 11.03 11.28 10.74 10.65

30969
624

AV
FAIL

10.24 10.24 10.52 10.68 10.65 11.16
10.49 10.57 11.00 11.06 11.10 12.53
10.11 10.13 10.16 10.49 0.0 10.31

30970
624

AV
FAIL

10.27 10.34 10.58 10.58 10.69 11.05
10.45 10.60 10.42 11.22 11.23 11.73
10.4 10.17 10.32 10.37 10.29 11.58

30971
624

AV
FAIL

10.21 10.24 10.31 10.40 11.05 11.82
10.30 10.42 10.64 10.81 11.03 11.12
10.12 10.06 10.08 10.05 12.46 0.06

30972
394

AV
FAIL

10.18 10.18 10.25 10.28 10.34 11.84 11.36
10.44 10.50 10.67 11.89 11.78 11.66 11.30
10.09 10.12 10.10 11.04 11.10 11.28 11.52

30973
394

AV
FAIL

10.22 10.61 10.60 11.00 11.97 11.39 11.19
10.53 11.92 11.97 11.02 11.92 11.29 11.77
10.51 10.34 10.34 11.10 11.34 10.61 11.23

30974
394

AV
FAIL

10.16 10.19 10.34 10.44 11.44 11.32 11.83
10.27 10.32 11.12 11.13 11.16 12.83 11.39
10.08 10.03 11.02 11.008 10.02 10.08 10.27

30975
624

AV
FAIL

10.07 10.07 10.08 10.08 11.60 12.03
10.19 10.22 10.24 10.42 10.57 11.62
0.0 10.01 0.0 10.03 11.77 10.67

30976
624

AV
FAIL

10.09 10.11 10.10 10.08 11.19 11.46
10.21 10.20 11.20 10.10 10.20 11.72
0.0 0.0 10.10 10.05 10.84 11.65

30977
624

AV
FAIL

10.09 10.09 10.09 10.09 11.62
10.11 10.11 10.16 10.21 10.25 11.62
0.0 10.02 10.01 10.03 11.37 10.40

30978
624

AV
FAIL

10.09 10.09 10.09 10.09 11.62
10.11 10.11 10.16 10.21 10.25 11.62
0.0 10.02 10.01 10.03 11.37 10.40

30979
624

AV
FAIL

10.09 10.09 10.09 10.09 11.62
10.11 10.11 10.16 10.21 10.25 11.62
0.0 10.02 10.01 10.03 11.37 10.40

30980
624

AV
FAIL

10.09 10.09 10.09 10.09 11.62
10.11 10.11 10.16 10.21 10.25 11.62
0.0 10.02 10.01 10.03 11.37 10.40

30981
624

AV
FAIL

10.09 10.09 10.09 10.09 11.62
10.11 10.11 10.16 10.21 10.25 11.62
0.0 10.02 10.01 10.03 11.37 10.40

100K
03737
□
100K

100K
03738
□
100K

AS GROUPS

98-100% R₀ @ 532 REPEAT

		40	100	200	300	200	100	200
100K	—	+0.21	+0.30	+2.45	+7.96	+5.24	+0.57	
03739	—	+0.58	+0.94	+0.95	+1.51	307	-4.62	
□	—	-0.06	-0.26	-8.90	-18.34	-13.78	-16.49	
NOHARD		0	0	0	5X	2	3	

100K	—	+0.07	+6.09	+6.37	+1.58	1.74	+2.71	
03738	—	+0.17	+4.72	+5.21	+5.63	6.01	+6.82	
□	—	-0.03	+0.08	+0.26	+0.36	0.42	+0.70	
✓2010		0	0	0	0	0	0	

2

* GROUPS CANCELLED TO BE REPEATED

PREPARED BY

CHECKED BY

APPROVED BY

TITLE MOISTURE-LOAD MATRAX - 1/8 W, 1/4 W - 100, 1000

CONTRACT PROJECT 88-2-20

98-100% RH @ 55°C

RESISTANCE

DATA NO.

		48	100	200	300	750	1000	2000			
30978	AV	±0.26	±0.22	±0.49	±0.28	±0.36	±0.38	±0.64			
100Ω	SPAN	±0.20	±0.10	±0.50	±0.20	±0.60	±0.60	±1.90			
1/8 W	FAIL	-1.00	-1.00	-1.00	-1.00	-1.00	-0.09	-1.40			
	AV	0	0	0	0	0	0	0			
30979	AV	±0.18	±0.21	±0.16	±0.16	±0.18	±0.11	±0.32			
100Ω	SPAN	±0.20	±0.20	±0.50	±0.10	±0.60	±0.10	±0.80			
1/8 W	FAIL	-0.20	-0.20	-0.20	-0.20	-0.20	-0.20	-0.10			
	AV	0	0	0	0	0	0	0			
30980	AV	±0.06	±0.12	±0.16	±0.21	±0.21	±0.24	±0.42			
100Ω	SPAN	±0.10	±0.10	±0.20	±0.10	0.0	±0.10	±1.11			
1/8 W	FAIL	-0.20	-0.20	-0.20	-0.20	-0.20	-0.20	-0.10			
	AV	0	0	0	0	0	0	0			
30981	AV	±0.16	±0.23	±0.24	±0.22	±0.60	±1.55				100.2
100Ω	SPAN	±0.20	±0.10	±0.12	±0.20	-0.06	±0.20				04694
1/8 W	FAIL	0	0	0	0	0	0				1/8 W
30982	AV	±0.15	±0.21	±0.26	±0.29	±0.31	±1.65				100.0
100Ω	SPAN	±0.20	±0.10	±0.12	±0.20	±0.14	±0.24				04695
1/8 W	FAIL	0	0	0	0	0	0				1/8 W
30983	AV	±0.23	±0.32	±0.52	±0.68	±0.58	±1.47				100.2
100Ω	SPAN	±0.53	±1.12	±1.31	±1.33	±1.19	±2.40				04696
1/8 W	FAIL	0	0	0	0	0	0				1/8 W
30984	AV	±0.22	±0.26	±0.28	±0.29	±0.15	±0.31	±0.91			
100Ω	SPAN	±0.80	±0.60	±0.60	±0.60	±0.20	±0.99	±1.50			
1/8 W	FAIL	-0.69	-0.89	-0.69	-0.79	-0.69	-0.79	-0.30			
	AV	0	0	0	0	0	0	0			
30985	AV	±0.02	±0.13	±0.12	±0.14	±0.12	±0.10	±0.43			
100Ω	SPAN	±0.10	±0.10	±0.10	±0.20	±0.10	±0.79	±1.02			
1/8 W	FAIL	-0.10	-0.82	-0.82	-0.82	-0.82	-0.82	0.0			
	AV	0	0	0	0	0	0	0			
30986	AV	±0.28	±0.33	±0.29	±0.30	±0.21	±0.20	±0.51			
100Ω	SPAN	±0.0	±0.50	±0.40	±0.30	±0.10	±0.70	±0.90			
1/8 W	FAIL	-1.00	-1.00	-1.00	-1.00	-1.09	-0.69	-0.49			
	AV	0	0	0	0	0	0	0			
30987	AV	±0.17	±0.28	±0.34	±0.32	±0.74	±2.68				100.0
100Ω	SPAN	±0.33	±0.50	±0.81	±1.54	±1.25	±6.82				04697
1/8 W	FAIL	-0.04	±0.02	±0.13	±0.25	±0.33	±1.15				1/8 W
	AV	0	0	0	0	0	0				
30988	AV	±0.19	±0.20	±0.38	±1.05	±0.89	±2.02				100.0
100Ω	SPAN	±0.39	±0.81	±1.25	±2.42	±2.22	±3.76				04698
1/8 W	FAIL	-0.01	±0.01	±0.10	±0.20	±0.03	±0.30				1/8 W
	AV	0	0	0	0	0	0				
30989	AV	±0.29	±0.43	±0.77	±1.22	±1.12	±2.00				100.0
100Ω	SPAN	±0.49	±1.22	±2.66	±3.74	±3.60	±4.28				04699
1/8 W	FAIL	±0.07	±0.06	±0.17	±0.27	±0.25	±0.57				1/8 W
	AV	0	0	0	0	0	0				

* GROUPS CANCELLED

4w - 10w, 10w

HOLD PAPER - 200. 66-6

TYPE

200. 66-6

FIGURE 80

8

DATE

10-10% R & C 200 2000

200	400	600	800	1000	1200	1400	1600	1800	2000
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100.2	±0.04	±0.26	±0.17	±0.05	±0.05	±0.09	±0.10
04694	+0.07	+1.45	+1.45	+0.07	+0.07	+0.07	+0.10
	-0.07	-1.41	-1.40	-0.06	-0.07	-0.81	-0.68
1/8 W	0	0	0	0	0	0	0
100.0	±0.30	±0.70	±0.68	±0.05	±0.05	±0.08	±0.10
	+0.10	+2.15	+2.15	+0.09	+0.11	+0.12	+0.15
04685	-0.06	-2.08	-2.05	-0.09	-0.08	-0.07	-0.0
1/8 W	0	0	0	0	0	0	0
100.12	±0.06	±0.32	±0.32	±0.05	±0.06	±0.05	±0.05
	+0.10	+0.61	+0.61	+0.10	+0.10	+0.10	+0.11
04696	-0.10	-0.44	-0.44	-0.10	-0.12	-0.17	-0.09
1/8 W	0	0	0	0	0	0	0

100.12	±0.04	±0.83	±1.83	±0.07	±0.06	±0.06	±0.10
04697	+0.09	+2.30	+2.36	+0.10	+0.14	+0.14	+0.77
	-0.07	-2.14	-2.12	-0.13	-0.10	-0.07	-0.06
1/4 W	0	0	0	0	0	0	0
100.12	±0.03	±1.11	±1.10	±0.05	±0.05	±0.08	±0.07
04698	+0.08	+3.47	+3.47	+0.14	+0.14	+0.15	+0.28
	-0.08	-3.29	-3.27	-0.09	-0.10	-0.03	-0.07
1/4 W	0	0	0	0	0	0	0
100.12	±0.03	±0.25	±0.25	±0.05	±0.04	±0.04	±0.08
04699	+0.0	+1.25	+1.25	+0.03	+0.03	+0.08	+0.30
	-0.10	-1.21	-1.19	-0.10	-0.10	-0.08	-0.09
1/4 W	0	0	0	0	0	0	0

2

OURS CANCELLED TO BE REPEATED

File 66-6

R6

RATE

FIGURE 31

8W 14W - 37K, 62K - 100K

TYPE	DWG. NO. 8	SHEET 32
R ₀	DATE	

Prod. 66-6

□ = 144 HRS.

98-100% RH @ 55C ~~Reprints~~

Part	48	100	200	500	750	1000	2000
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100K	—	±0.07	+0.10	+1.29	+0.24	±0.29	10.30
03237	—	+0.17	+0.23	+3.18	+0.47	0.56	10.91
□	—	-0.03	0.0	-2.71	+0.07	-0.12	10.16
1/8W	—	0	0	0	0	0	0

100K	—	±0.09	±0.08	±0.08	±0.10	±0.13	10.35
03236	—	+0.06	+0.11	+0.20	+0.30	0.40	10.82
□	—	-0.24	-0.20	-0.11	-0.05	-0.02	10.14
1/4W	—	0	0	0	0	0	0

2 GROUPS CANCELLED TO BE REPEATED

2

TITLE SUMMARY OF MIL-R-11E PERFORMANCE CHARACTERISTICS
CONTRACT PROJECT 88-71-20

14.0%	0.035	104	30	40	140 Ave 130000 10000
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RESISTANCE - TEMPERATURE CHARACTERISTIC	VOLTAGE	CIRCUIT RESISTANCE	POSITION RESISTANCE	DATA	TEMP. POSITION	OPERATING TEMPERATURE	MOISTURE RESISTANCE	
							1	2

7

CHARACTERISTICS

G-67-289 A

TYPE

R₂ 1/4

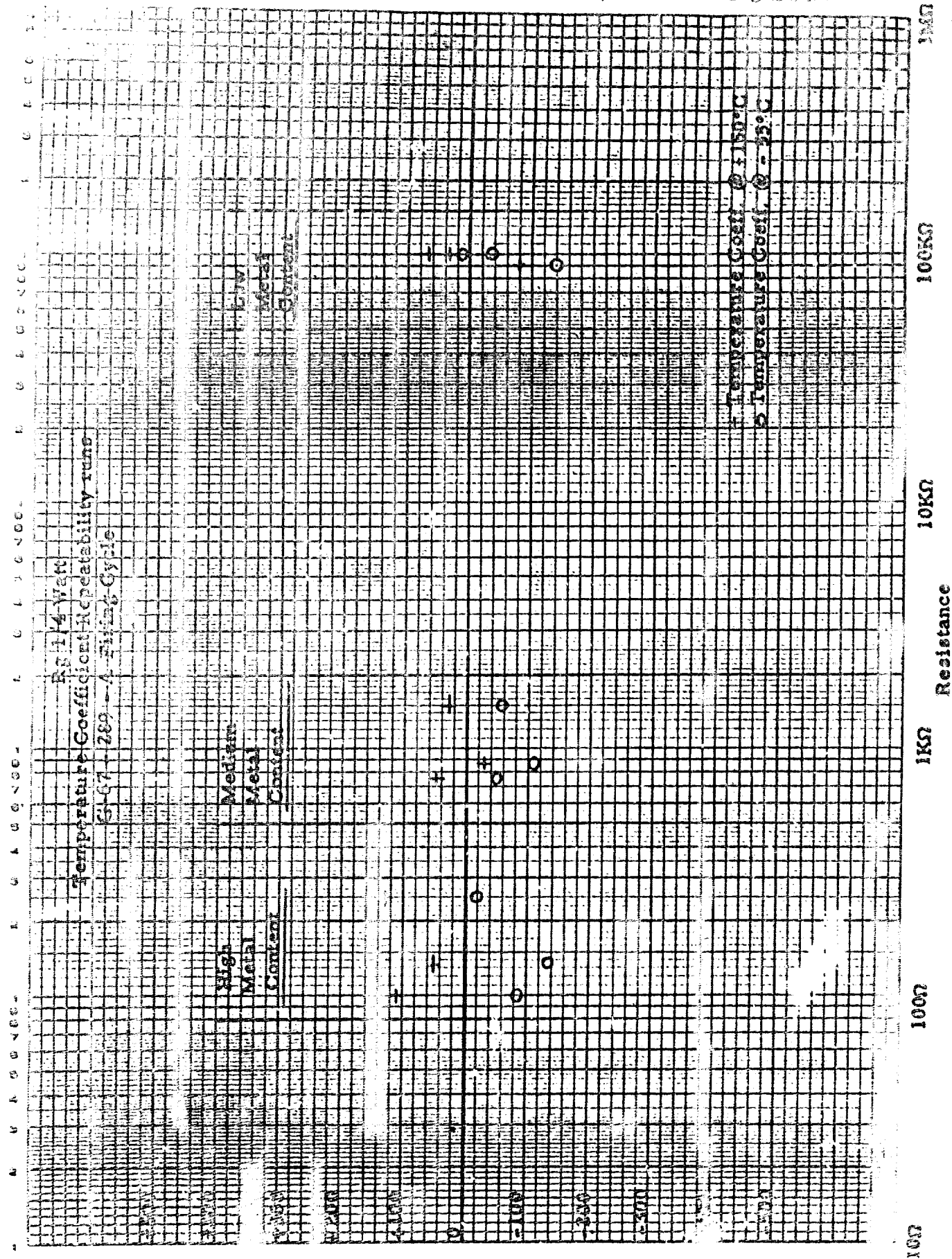
B- Figure 33

DATE - 11-15-65

TEMPERATURE CYCLE		160 AVE, 15.0 AVE 10" H I 2				MOISTURE RESISTANCE		DATA #2	70° LOAD LIFE HOURS					DATA #2	1.0		3.0		DATA #2	2.0		DATA #2	ISOLATION - ABILITY	
LOAD	NO LOAD	RESISTANCE (MESH)	NO LOAD	RESISTANCE (MESH)	SHORT TIME OVER LOAD	48	240		504	720	1008	TERMINAL STRENGTH	EFFECT OF SOLIDITY		SHOCK TEST	NO - FREQUENCY VIBRATION								
0.04	10.05	ALL	10.21	ALL	10.02	0	10.03	10.11	10.20	10.26	10.28	0	10.11	10.04	0	10.03	0.03							
0.08	10.12	10 ⁴	10.65	10 ⁴	10.04	0	10.08	10.25	10.48	10.60	10.63	0	10.19	10.20	0	10.06	0.06							
0.08	10.01	MESH	0.08	MESH	0.04	0	0.04	0.04	10.12	10.17	10.20	0	10.04	0.0	0	0.0	0.06							
0	9/5	9/5	9/5	9/5	0	0	0	0	0	0	0	0	0	0	0	0	0							
0.04	10.07	ALL	10.20	ALL	10.09	0	10.32	10.32	10.33	10.34	10.34	0	10.19	10.13	0	10.02	10.02							
0.07	10.02	10 ⁴	10.02	10 ⁴	10.03	0	10.04	10.07	10.19	10.21	10.23	0	10.16	10.13	0	10.04	10.06							
0.12	10.14	MESH	0.55	MESH	0.01	0	1.97	1.93	1.85	1.86	1.83	0	10.03	0.89	0	0.0	0.0							
0	9/5	9/5	9/5	9/5	0	0	0	0	0	0	0	0	1	0	0	0	0							
0.05	10.20	ALL	10.32	ALL	10.17	0	10.07	10.05	10.04	10.11	10.14	0	10.06	10.12										
0.16	10.24	10 ⁴	10.48	10 ⁴	10.10	0	10.10	10.30	10.57	10.41	10.47	0	10.12	10.12										
0.06	10.14	MESH	10.07	MESH	0.82	0	0.19	0.10	0.10	0.10	0.07	0	0.0	10.08										
0	9/5	9/5	9/5	9/5	0	0	0	0	0	0	0	0	9/9	9/9										

2

WASH DC
JAN 1968

Temperature Coefficient
°C./mm.

Best Available Copy

Unclassified

Security Classification

DOCUMENT CONTROL DATA - R&D

(Security classification of title, body of abstract and indexing classification must be entered when the special report is submitted)

1. ORIGINATING ACTIVITY (Corporate method)		2a. REPORT SECURITY CLASSIFICATION	
I R C 401 North Broad Street Philadelphia, Pennsylvania 19108		Unclassified	
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11. SUPPLEMENTARY NOTES		12. SPONSORING MILITARY ACTIVITY	
Reliable Resistor Development Report		U. S. Army Electronics Command Fort Monmouth, New Jersey AMSEL-KL-EC	
13. ABSTRACT			
<p>MIL-R-11 70°C load life tests have been completed to 1000 hours on the 100Ω group. The completed results, on all pertinent resistance values, demonstrates conformance to the MIL-R-11 requirements. The contract requirements of 5% maximum resistance change on the Mil moisture resistance and Resistance-Temperature characteristic of less than 500ppm/°C have also been met.</p> <p>The moisture load matrix has been completed through 2000 hours on the 100Ω and 100KΩ groups. These results definitely indicate smaller resistance changes with increasing load, especially in the 100KΩ group.</p> <p>The temperature load matrix tests have completed 2000 hours on the 100Ω group and 3000 hours on the 100KΩ group. The 10Ω, 1KΩ, 10KΩ, and 39KΩ groups have completed 6000 hours of testing. The present calculated failure rate, which includes the two early (50 hours of test) failures on the 100KΩ group, is 0.10%/1000 hours at a confidence level of 60% on units tested at 85°C ambient with 1/4 watt load. The calculated failure rate without the two early failures is no more than 0.03%/1000 hours at a confidence level of 60%. The average resistance change for the 100Ω and 100KΩ groups after 2000 hours at 85°C ambient with 1/4 watt load is less than 0.1%; and less than 0.4% on the 10Ω, 1KΩ, 10KΩ, and 39KΩ groups.</p>			

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14. KEY WORDS	LINK 1		LINK 2		LINK 3	
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Resistors General Purpose Reliable, Low Cost Stable Test Matrix Cermet Failure Rate Failure Mechanism Resistor Development						

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